MOUNT SELINA PROJECT
MONTAGU, TASMANIA
EL29/2002

SIX MONTH PROGRESS REPORT
31ST JANUARY 2006 TO 31 ST JULY 2006

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ABSTRACT

The following is a 'Progress Report on Exploration Activities' at Exploration Licence 29/2002, Mt Selina, for the six month period starting on the 31 January 2006 and finishing on the 31 July 2006'.

Activities during the six-month period include;

- Analysis of soil geochemical assays received from the soil geochemical programme finished late in January 2006.
- Validation and review of existing data before capturing it in proprietary Geoinformatics database systems (e.g. FracSIS) and carrying out three dimensional modelling of the data. Followed by target generation and ranking of targets using further proprietary software and systems (e.g. Monte Carlo).

The report has been written to meet any additional reporting requirements stemming from the six month deferral in exploration expenditure granted to the company by the MRT on the 21 December 2005.

All exploration activities are being conducted in an environmentally sensitive manner.

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1. INTRODUCTION

This report is a summary of the exploration activities conducted on the Mount Selina exploration licence for the period of 31st January 2006 to 31st July 2006.

The Mt Selina exploration license, number 29/2002 (Figure 1), was granted to Adamus Resources on 31 January 2002 as a 109km^2 area. The license was reduced in size at the end of the second year (2004) when 51km^2 were relinquished. The license is now 58km2 and is due to expire on the 31 January 2008.

In April 2005 Adamus Resources Limited and Bass Metals Limited entered into a Farm in and Joint Venture Agreement. Bass Metals will act as managers during the farm in period from a base at the Hellyer Mine site. Bass Metals was previously known as Resource Finance and Investments Limited (RFI).

At the end of the third year (2005) the department of MRT granted a six-month deferral in exploration expenditure from the 31 January 2006 to the 31 July 2006. This report has been written to meet any additional reporting requirements of the MRT due to this deferral.

1.1 Location:

The Mount Selina license is located between Queenstown and Rosebery, on the west coast of Tasmania (Figure 1). The licence is found on the Sophia and Franklin (1:100,000) map sheets. The licence area is topographically bounded to the north by Mount Murchison, south by the Comstock Valley, east by Sticht Ranges and the west by the Tyndall Ranges.

The north-western corner of the license is crossed by the sealed Anthony Road. Access to the central and southern areas is via gravel tracks maintained by the Hydro-Electric Corporation, Parks and Wildlife Service and Copper Mines of Tasmania. Access to the remainder of the licence is either on foot or by helicopter.

The majority of the licence is covered by the Tyndall Range Regional Reserve and the Lake Beatrice Conservation Area. Topographically the area is rugged and quite variable displaying steep wooded slopes, deeply incised valleys and grassed flat plateaus and broad plains. Numerous lakes and closed catchment basins are located throughout the licence area.

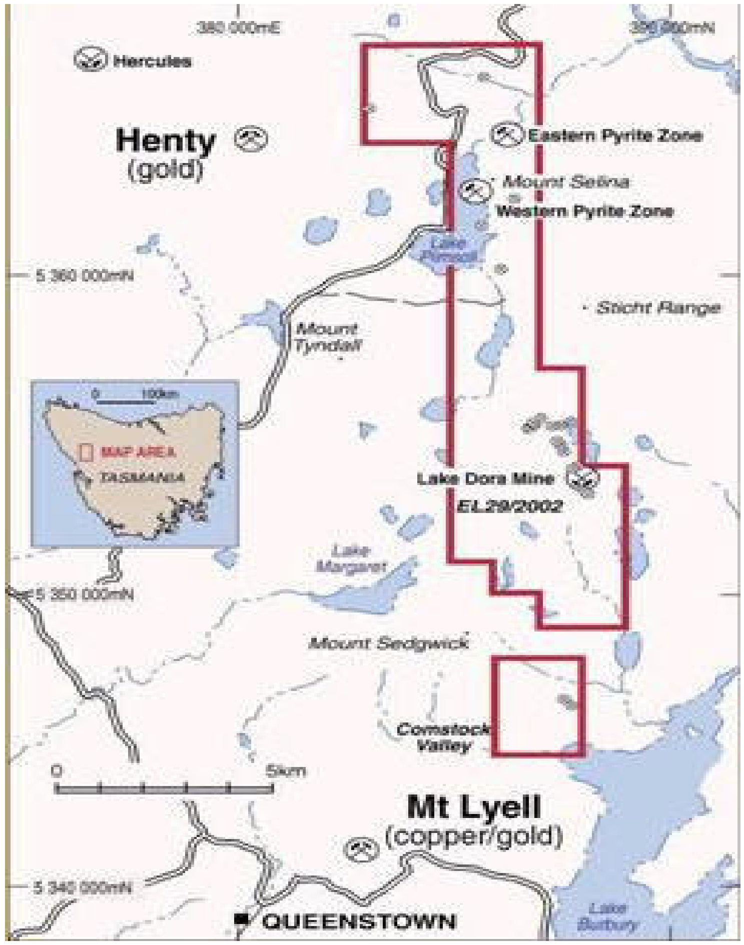

Figure 1. Mount Selina Licence (EL29/2002). Located in North-western Tasmania.

1.2 Geology Overview:

The oldest rocks in the region belong to the Proterozoic Tyennan Metamorphics. The Mt Read Volcanics ("MRV") lie unconformably on top of the Tyennan Metamorphics. The MRV provide the best stratigraphic target for finding polymetallic VHMS deposits. Owen group sediments overlay these volcaniclastic units in the central and western licence areas with alluvium and glacial deposits covering a large portion of the central and northern areas. The Murchison Granite, which can be seen in small outcrops within the licence, intrudes and underlies the Mt Read Volcanics (Rust 2004) (Figure 2).

1.2.1 The Mount Read Volcanics

The Mt Read Volcanics are a belt of volcaniclastics and sediments, of Mid- Cambrian age, which host the known mineralisation in the licence area. Along the eastern margin of the licence area outcrops of the Mt Read Volcanics basal units can be observed. These lower units are made up of the Eastern Quartz Phyric Sequence, the Central Volcanic Complex and the Tyndall Group (Rust 2004).

The Eastern Quartz-Phyric Sequence hosts the majority of historical copper workings on the licence. The majority of this sequence is comprised of felsic volcaniclastics, porphyries and intrusives, with minor units of shales and cherty mudstones (Rust 2004).

Within the north-western and southern areas of the licence units from the Central Volcanic Complex can be observed in outcrop. Hosting the Red Hills Cu-Pb-Zn-Au-Ag mineralisation this complex is composed of felsic volcanic rocks, rhyolite, dacite and shale and sandstone units containing volcaniclastic tuffs (Rust 2004).

Outcropping to the north of Mt Selina and then from Lake Dora to the south of the licence as a belt, the Tyndall Group hosts the zinc mineralisation of the Anthony and East Selina prospects. This group is comprised of volcaniclastic sandstone and conglomerate units which are in contact with the basal volcaniclastics of the Eastern Quartz-Phyric Sequence. The Tyndall Group is also present in the Henty Fault zone, to the west of the licences, as basal felsic volcanic rocks (Rust 2004).

1.2.2 The Owen Group

Generally a sequence of marine sediments, Cambrian to Ordovician in age, unconformably overlie the Mt Read Volcanics. This group is made up of a series of conglomerates, pebble conglomerates, breccias, sandstones, limestones, silts and shales (Rust 2004). It is not likely to host any exhalative styles of mineralisation such as Taylor and Mathison (1990) report for the younger Gordon Group. However, it could potentially host mineralisation associated with intrusion of Late Devonian–Early Carboniferous granitoids.

1.3 Exploration Rationale:

The area is famous for hosting the Rosebery (Pb-Zn) and Hellyer (Pb-Zn-Ag-Au) polymetallic VHMS deposits and the large-scale Mt Lyell copper ore bodies. EL29/2002 was acquired primarily to search for economic VHMS Au-Cu and Pb-Zn-Ag-Au deposits within the Mount Read Volcanic Belt.

Historically the area has been examined by a number of companies for potential VHMS deposits with limited work being conducted on the gold potential of the region. Previous companies believed that the licence area was not likely to be the host of any large-scale, economic VHMS base metal deposits.

Historically poor gold exploration results from the licence are thought to be a direct function of the exploration focus being on base metal VHMS-style mineralisation. There is evidence from the licence area of gold assays returning as high as 48.8g/t. Also in the Henty/Mt Julia area there are some high grade gold deposits in the order of <500,000t @ 10-30g/t.

It is felt that the region is still prospective for both economic VHMS Au-Cu and Pb-Zn-Ag-Au deposits and exploration works will focus on these styles of mineralisation.

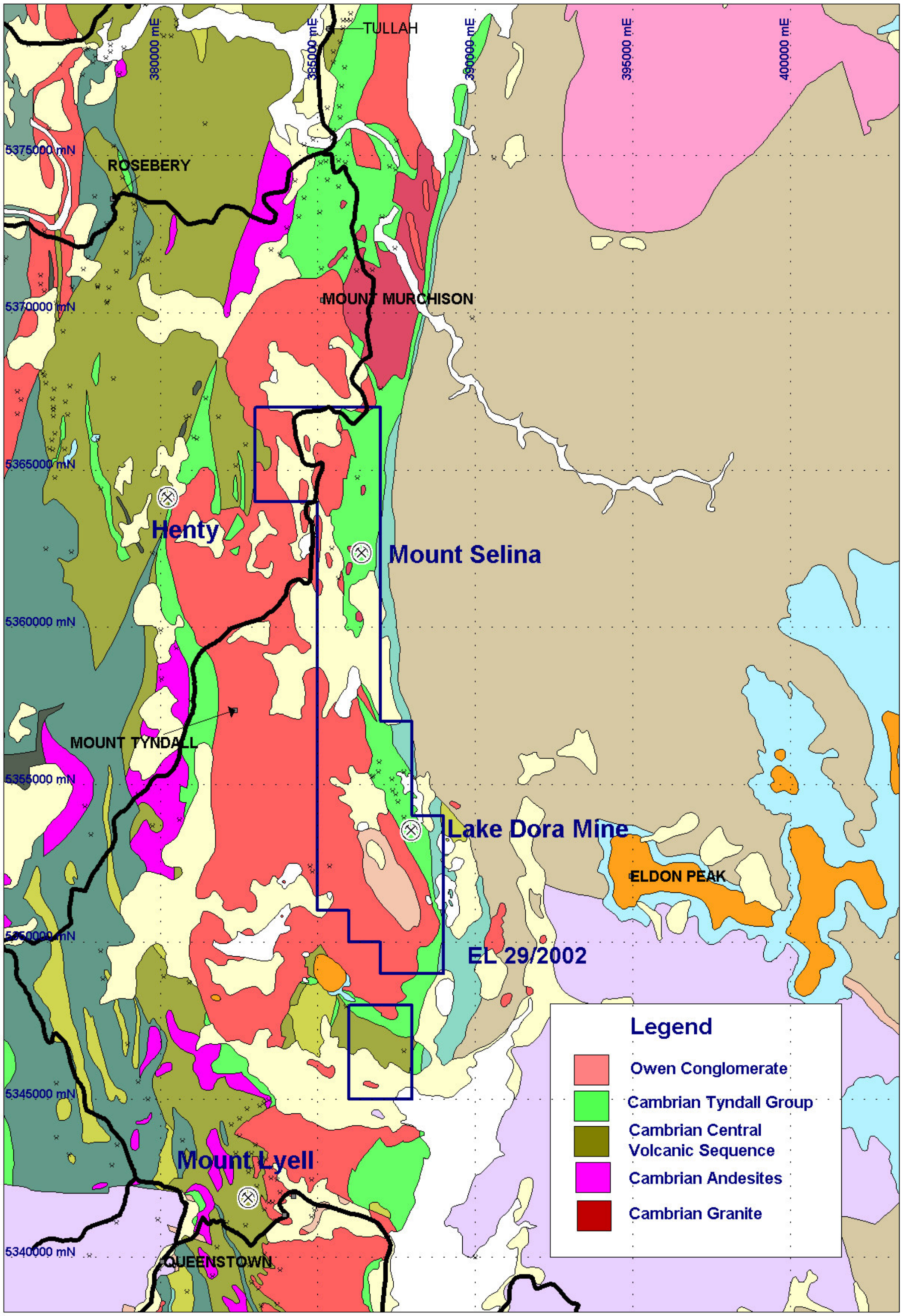

Figure 2. Regional Geology showing licence boundaries, roads and towns.

2. WORK COMPLETED

2.1 Historical Mining:

The discovery of the Lake Dora and Red Hills mineral fields, in 1891, brought about the beginning of historical work in the area. Efforts at this time basically consisted of small to moderate scale prospecting and limited mining attempts. Historically copper was the main element of interest.

The Lake Dora area was worked with only moderate success through a series of trenches and prospecting shafts and tunnels. Early workers noted the presence of cobalt in the region and copper and silver were the main elements of economic interest. In 1908 the Lake Dora field was abandoned due to poor copper grades.

There is very little recorded activity in the region from 1908 until the beginning of modern exploration efforts in the late 1950's.

2.2 Exploration Prior to Current Licence:

Modern exploration efforts in the Mt Selina region commenced in the late 1950's (Figure 3). Prior to this only limited prospecting and mining took place. The following history of modern exploration in the Mt Selina licence has been taken from Rust (2004):

Date: 1957 - 1962
Company: Rio Tinto Australian Exploration Pty Ltd
Exploration Philosophy: Focus on locating large-scale, economic Cu, Zn, Pb, Sn mineralisation utilising geophysical methods, mapping and stream sediment sampling.
Work Completed: Examined the Lake Selina, Lake Dora, Lake Spicer, West Sedgwick, Comstock Valley and Red Hills areas for potential to host large-scale Cu, Zn, Pb, Sn mineralisation. Aeromagnetic surveys and four diamond drill holes were completed over the Red hills area.
Results and Conclusions: No results are recorded.

Date: 1966 - 1987
Company: MLM&RC and Goldfields Exploration Pty Ltd (both subsidiaries of Renison Goldfields Consolidated Ltd)
Exploration Philosophy: Initially targeting Mt Lyell analogous copper mineralisation and later expanded to incorporate VHMS base metals with a more recent focus on gold mineralisation.
Work Completed: Assessment and interpretation of previous aeromagnetic surveys (for target generation), stream sediment, soil and rock chip sampling, induced polarization surveys, resistivity and ground magnetics surveys, mapping, diamond drilling, trace element and Ni:Co drill core studies, EM and UTEM ground level geophysical surveys.
Results and Conclusions: several targets generated however follow up drilling generally only returned low grade anomalous results. Area shows large anomalous zones of Cu-Pb-Zn-Ag±Au.

Date: 1985 - 1995
Company: CRA Exploration and Aberfoyle Resources Ltd Joint Venture
Exploration Philosophy: Generally focused on base metals, however the southern areas were explored for base metals and gold due to structural and lithological similarities between the area and the Red Hills Pb-Zn-Au deposit.
Work Completed: Ground based magnetic surveys, mapping, stream sediment, soil and

rock chip sampling, diamond drilling and a downhole EM survey.
Results and Conclusions: Limited exploration targets generated, previous anomalies confirmed however further work failed to increase the economic potential of the anomalies. Some interesting anomalous results returned from rock chip samples showing elevated Au, Pb and Zn assays.

Date: 1987 - 1998
Company: Aberfoyle Resources Ltd
Exploration Philosophy: Exploration for VHMS deposits at +200m depth. Main elements of interest were Pb-Zn and gold to a lesser degree.
Work Completed: Ground magnetic surveys, mapping, rock chip sampling and drilling.
Results and Conclusions: Work returned some anomalous Au, Ag, Cu and Pb grades, however overall Pb, Zn and Au values were poor.

Date: 1996 - 1997
Company: Copper Mines of Tasmania Pty Ltd
Exploration Philosophy: Targeting VHMS base metals, gold or disseminated sulphide deposits. The exploration area was selected as it was considered to be analogous with the Red Hills Rhyolite Dome.
Work Completed: Stream sediment and rock chip sampling.
Results and Conclusions: Results returned from the programs were variable with some Au, Zn, Cu and Pb point anomalies defined.

Date: 1996 - 2001
Company: Pasminco Exploration Ltd
Exploration Philosophy: exploring for VHMS Pb-Zn-Cu-Au-Ag deposits using the Rosebery/Hellyer deposits as the conceptual model. Also concentrating on large tonnage, intrusive related Cu-Au systems and vent-breccia style "Leyshon" Au.
Work Completed: Literature review, helicopter supported reconnaissance, re-assaying of diamond drill holes, mapping, rock chip and soil sampling and Pb isotope studies.
Results and Conclusions: Re-assaying of diamond drill holes returned disappointing results. However rock chip sampling showed significant Au, Cu, Pb, Zn, Ag and Co anomalism from narrow veins. Several anomalous (6-37 g/t) Ag assays were returned.

Date: 1998 - 2002
Company: Goldfields Exploration
Exploration Philosophy: Unsure
Work Completed: None
Results and Conclusions: The Mt Selina ground was held in conjunction with another area. Goldfields concentrated exploration efforts on the other ground. The Mt Selina portion was released due to increasing expense commitments without any work being conducted on it.

The exploration conducted by previous companies had highlighted the following targets: the Eastern Pyrite Zone, Anthony, the Western Pyrite Zone and some geophysical targets at Lake Dora, Lake Spicer and Beatrice Dome.

Previous exploration efforts generally focused on Rosebery/Hellyer style VHMS deposits and Mt Lyell style copper deposits as the conceptual target. As a result the elements of primary interest have been the base metals Pb, Zn and Cu with later limited focus on Au.

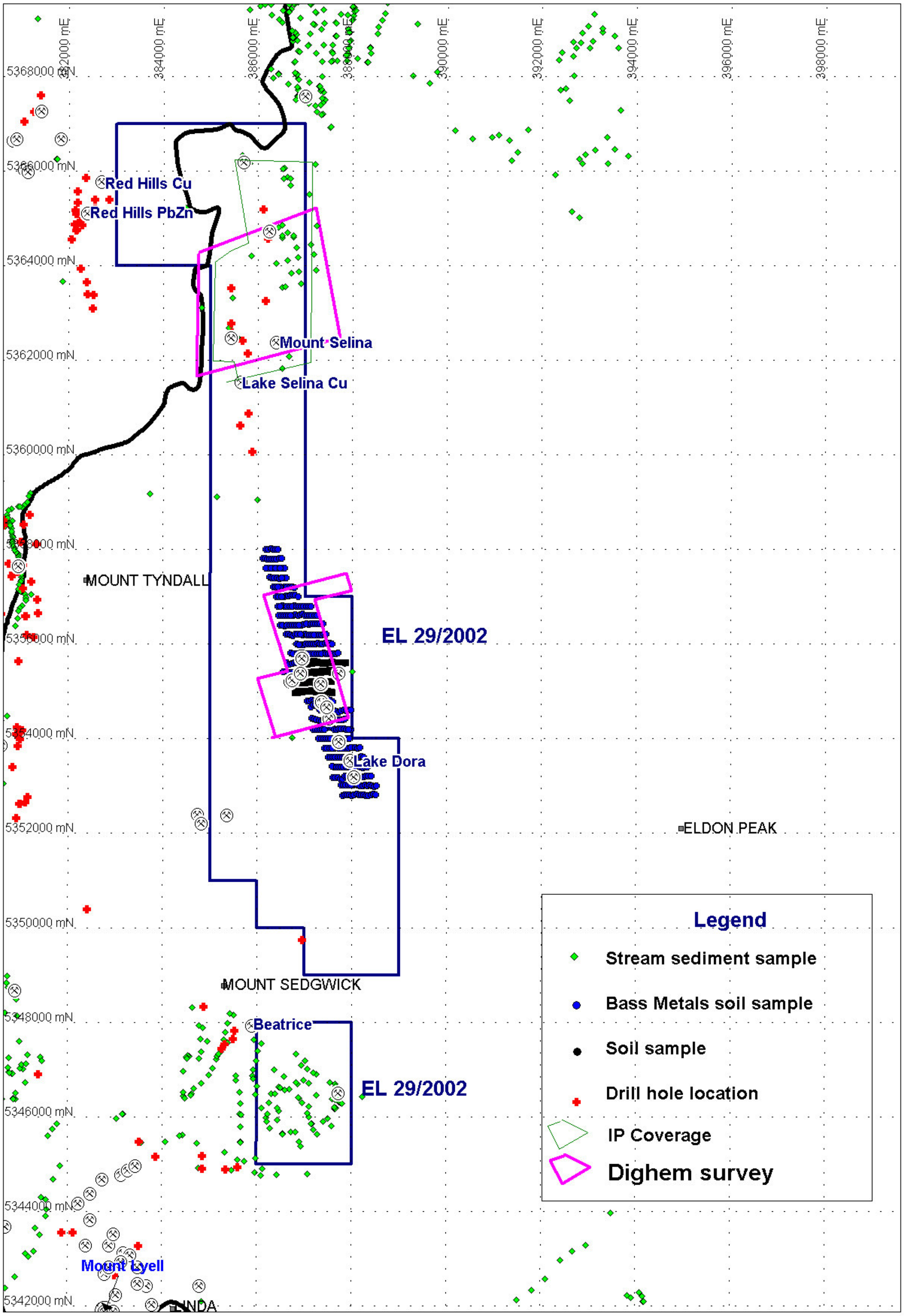

Figure 3. Historical Exploration Activity Map.

2.3 During Current Licence Pre 31st January 2006:

- Adamus conducted gridding and soil sampling over selected targets
- Establish exploration base at Hellyer Mine Site.
- Compilation of historical data available from open file sources into a MapInfo database and processing of ASTER satellite data.
- Bass commenced gridding and soil sampling over two prospective areas.

3. EXPLORATION COMPLETED 31 JANUARY 06 TO 31 JULY 06

The below section reports on exploration conducted between the 31 January and the 31 July 2006. This essentially involved; (1) analysis of soil geochemistry assays received from the programme finished in January 2006, and (2) compilation of data into a proprietary Geoinformatics database before 3-dimensional modelling of the data and target generation was carried out.

Geochemistry Programme Results

A soil geochemical programme was conducted through to the end of January 2006. The results for this program did not become available until February-April 2006. The program was conducted in two areas in the Selina licence. Area 1 was between Lake Rolleston-Lake Dora and Area 2 was between Lake Dora-Lake Spice. The program involved the collection of samples from a grid with 200 metre spaced minimum impact cut-lines and samples spaced 50 metres apart. A Honda Big Red quad bike was used as transport to and from the general sampling area on a daily basis.

Samples were collected using a hand auger. Samples varied from 0.8kg to 2.55kg in weight. At all times during the cutting of grids and collecting of samples care was taken to avoid the transfer of soil or vegetation. With tools, shoes and clothing being cleaned of loose soil or vegetation after each sample was collected to minimize the transport of noxious weeds and plant diseases. For a more detailed account of the sampling procedures refer to the 'Mt Selina Annual Progress Report on Exploration Activities 31 January 2005 to 30 January 2006'.

Normalising and then summing groups of metals that are commonly associated (eg Pb-Zn-Ag, Pb-Zn, Cu-Zn, Cu-Zn-Au, Cu-Au) identified one main anomaly. This anomaly is found to the north of the Lake Dora Mine trend (North Lake Dora) and almost immediately south east of Lake Rolleston. It is defined by a coincident 681ppm lead and 521ppm zinc anomaly as well as a small internal gold anomaly. Refer to Appendix 1 for assay results from the soil geochemical programme. Refer to Appendix 3 for digital files containing the data in text file format.

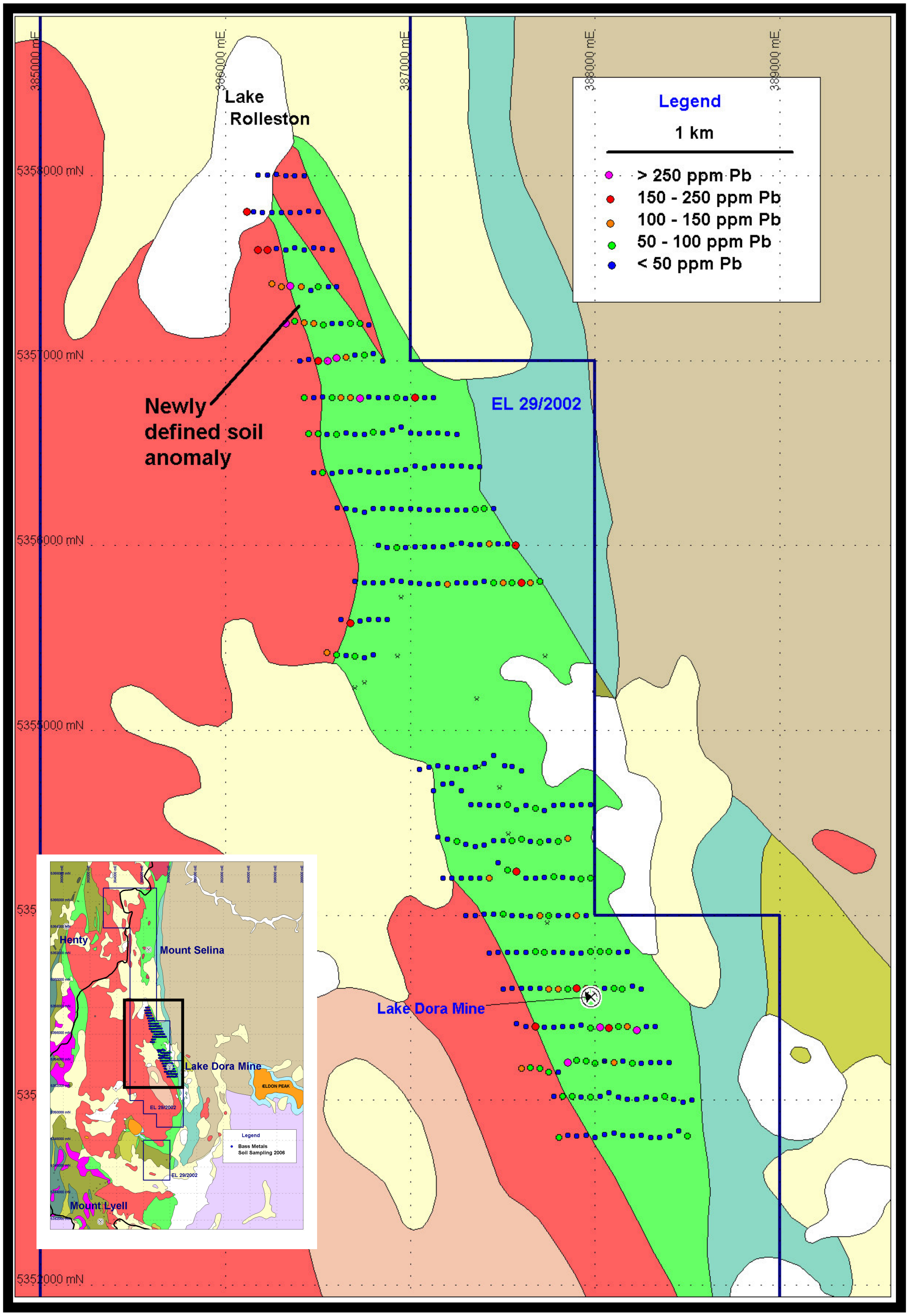

Figure 4. Soil Geochemical Programme – lead assays.

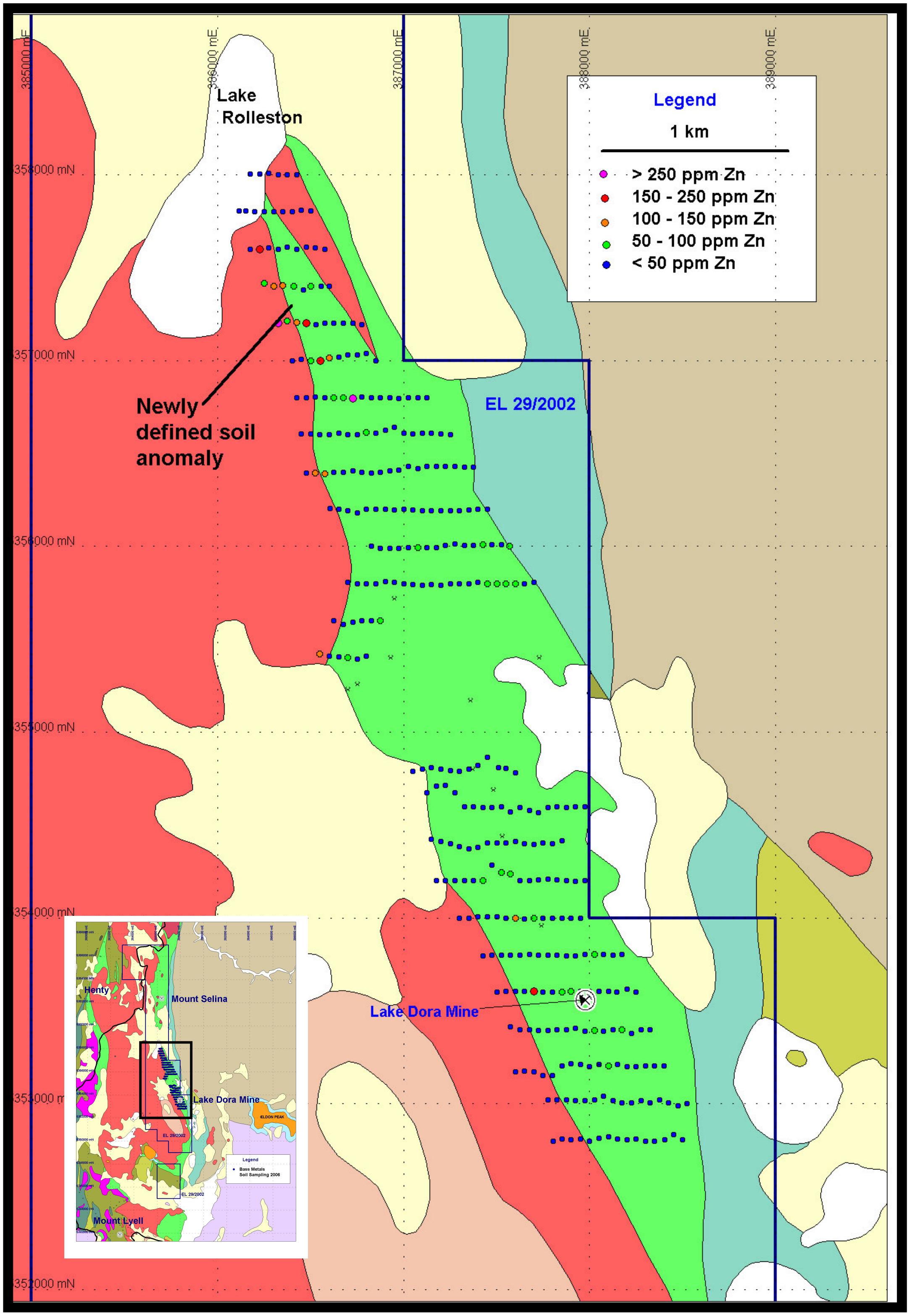

Figure 5. Soil Geochemical Programme – zinc assays.

Geoinformatics Geological Modelling & Targeting

The Geoinformatics process involves the efficient capture of historical data in proprietary Geoinformatics database and software systems (eg IFS & FracSIS). Proprietary software and methods are then used to generate 3-dimensional geological models and targets (Monte Carlo Ranking). The Mt Selina work is part of a larger 'Intervention Project' called the MRVIP (Mount Read Volcanics Intervention Project - stage 1b). The Stage –1b Project focuses on all of Bass Metals 13 regional licences. A final Stage-2 Project focused on regional target generation without consideration of licence boundaries though is not reported on here.

The Stage 1b Project attempts to incorporate Geoinformatics understanding of the three dimensional controls on world class VHMS mineralization to rapidly provide Bass with high-quality targets in the Mt Selina licence for rapid drill testing and other areas for follow-up field work including soil type geochemistry. Models were also developed for the targeting of intrusive related Sn systems (e.g. Renison and Mt Bischoff) and intrusive related Ni-skarn systems (e.g. Avebury). Targets were identified and ranked according to probabilistic Monte Carlo analysis of best-available 3D and 2D geoscientific data and allowed an assessment of exploration risk and uncertainty.

Much of the data for the project was obtained from open file reports. A data audit of 1,300 reports was completed by Dan Core, Graeme Cameron, Neville Panizza and Helen Ly. Work on the Stage 1b Project commenced in early February 2006 and was largely complete by July 2006. A target workshop with alliance personnel was held at Hellyer in July 2006 and final targets are being delivered in August 2006.

At Mt Selina Geoinformatics generated a total of 16 Mount Lyell style and 22 Rosebery style VHMS targets (Figure 6). Most targets ran down the eastern side of the licence area where they identified prospective portions of the Mt Read Volcanics. The western side of the licence has outcropping Owen Group sediments.

Comparing results from Bass's 2006 soil geochemical programme with the Geoinformatics geological model confirmed the prospectivity of the North Lake Dora soil geochemical anomaly (Figure 7). Refer to Appendix 3 for a summary of the Geoinformatics methodology.

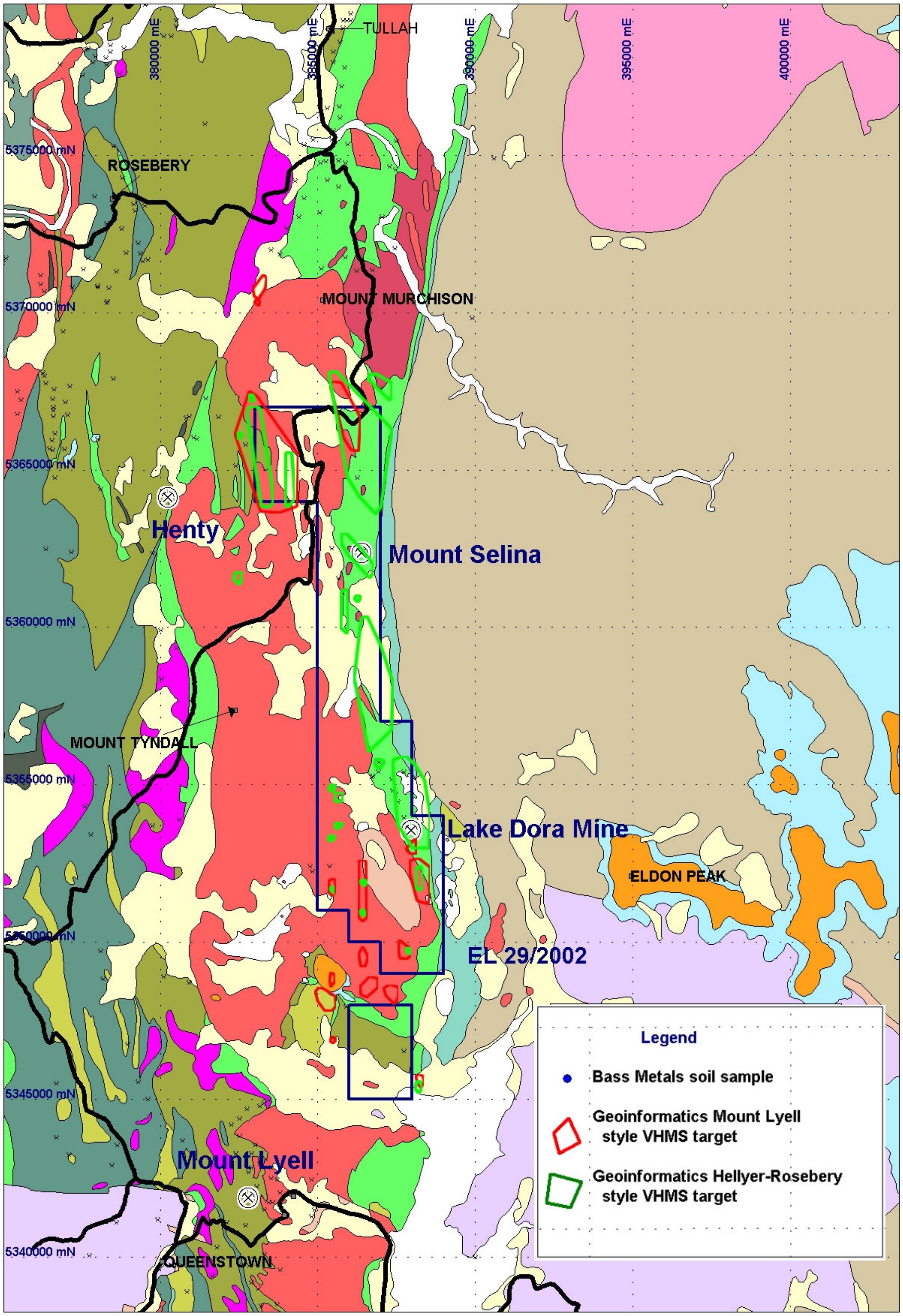

Figure 6. Geoinformatics - VHMS Targets overlain on geological model.

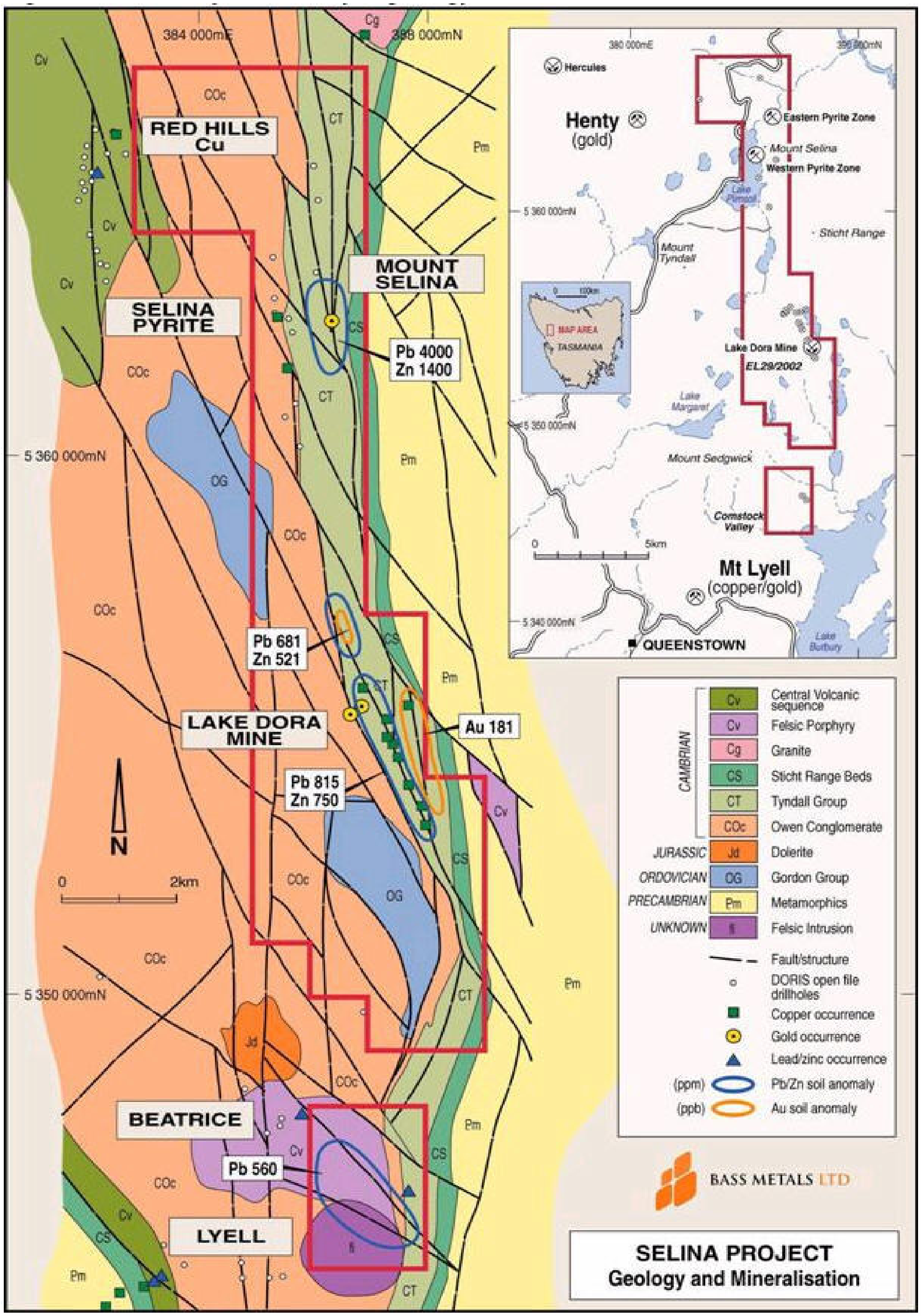

Figure 7. Geochemical anomalies overlain on a Geoinformatics geological model.

4. PROPOSED EXPLORATION

The proposed work program for the Selina licence includes infill soil sampling, ground geophysics along soil lines and drill testing of the main anomaly.

A program of 85 soil samples has been planned to infill the main zone of Pb-Zn soil anomalism south of Lake Rolleston. Following evaluation of the infill soil sampling results a ground EM / IP program to further define the area of base metal anomalism is envisaged prior to drill testing of the target via two 200m deep diamond drill holes.

Budget

Geologist & Technicians Time ($800 day)	$10,000
Line clearing ($2,000 /km)	$8,000
Soil sampling ($120 / sample)	$10,200
Geophysics (Ground or down hole)	$15,000
Drilling (400m @ $180/m)	$72,000
Assaying ($20 sample)	$8,000
Total	**$123,200**

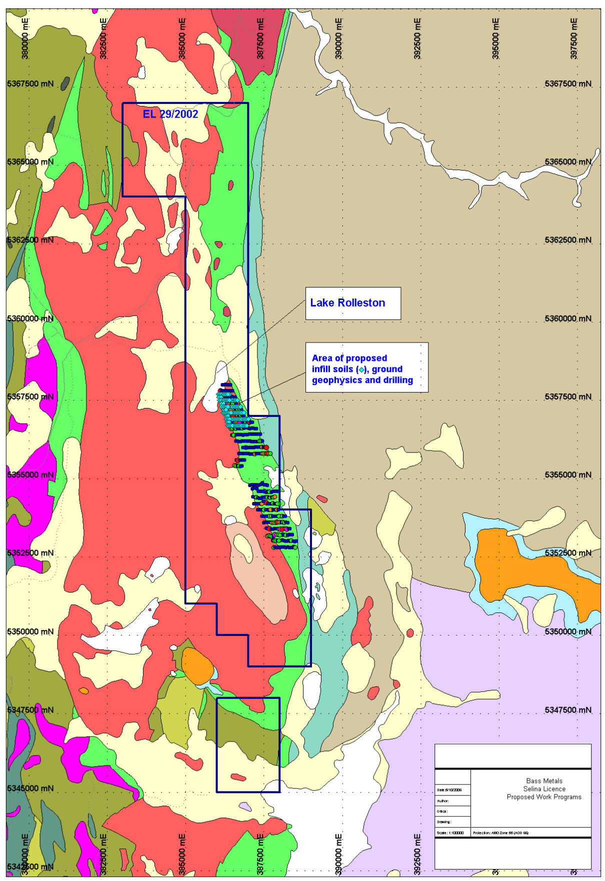

Figure 8. Location of proposed infill soil sampling, geophysical and drilling programmes.

5. ENVIRONMENT

Approximately 18km of line cutting has been completed on the southern portion of the Mt Selina licence to allow further soil sampling to be conducted (Figure 9). All lines were cut at an angle to existing tracks. Only existing tracks will be accessed by 4WD Utility motorbikes.

Prior to starting the program all staff were made aware of the importance of minimizing the impact that exploration activities had on the environment and the risks associated with spreading plant diseases and weeds as a result of day to day exploration tasks.

Following the completion of soil sampling all sample sites were infilled and rehabilitated and all rubbish was removed from the area. The gridlines that were cut have been partially covered so as to allow access at a later date should it be required. If no further access is deemed necessary lines will be rehabilitated in the manner required by the relevant state legislation.

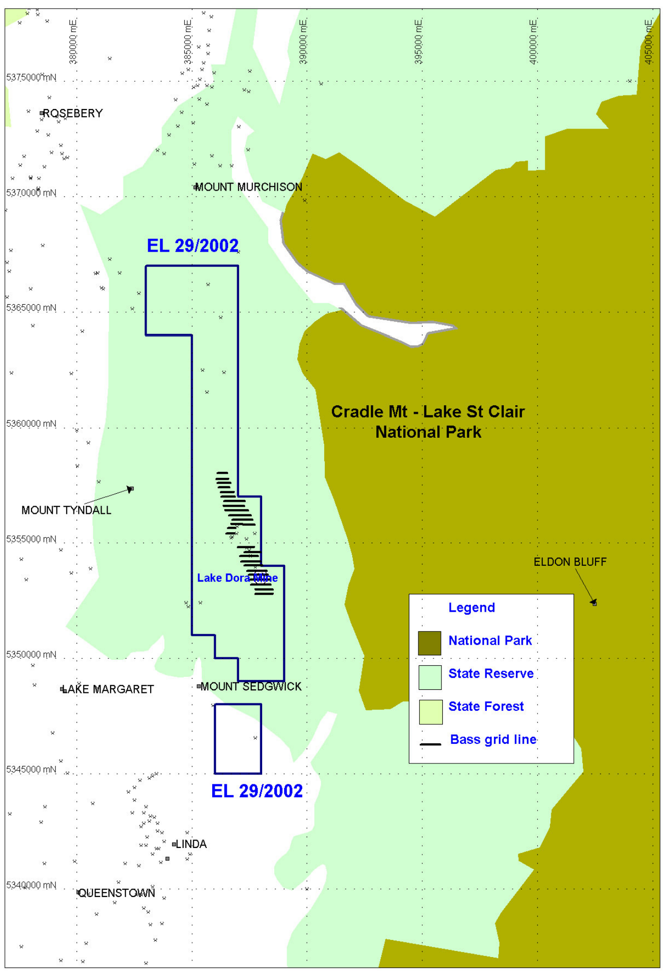

Figure 9. Environmental Activity Map showing grid lines cut in January 2006.

6. EXPENDITURE

Period Ending	Mar-06	Jun-06	Jul-06	Eligible Totals
Administration	7,499.04	4,444.07		**11,943.11**
Geology-Personnel & Overheads.	2,560.16	32,798.09[1]	7,938.00[1]	**43,296.25[1]**
Gridding	38,300.00			**38,300.00**
Geochemistry	26,570.10	7,102.55	85.00	**33,757.65**
Geophysics				
Drilling				
Feasibility Studies				
Rehabilitation				
Other – Safety Equip	61.15	96.08		**157.23**
Adjustment (Admin<10%)				
Total - Eligible	74,990.45	44,440.79	8,023.00	**127,454.24**
Cumulative Total	**128,749.59**	**173,190.38**	**181,213.38**	

Table 1. Expenditure 31 January 2006 to 31 July 2006.

*1 includes Geoinformatics costs.

The MRT granted Bass Metals a deferral in expenditure from the 31 January 2006 to the 31 July 2006, on the 21 December 2005.

The major part of the expenditure during the period is related to completion of the soil geochemical programme commenced in early 2006 and the Geoinformatics ‘MRV Stage 1b- work undertaken on the Selina Licence.

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APPENDIX 1

(Six Monthly Report)

Soil Geochemical Sample Locations

GRID	LINE	NO.	DEPTH	EASTING		NORTHING		COLOR	QTZ	SOIL	PEAT	CLAY	COMMENTS
SAMPLE NUMBER			DEC							PROFILE	SANDY	GRAVEL	
DS	-48	1	4	387	50	535	4790	BROWN	0%	C	PEAT		
DS	-48	2	6	387	100	535	4800	BROWN	0%	C	PEAT		
DS	-48	3	5	387	150	535	4810	BROWN	15%	C	SANDY	CLAY	
DS	-48	4	2	387	200	535	4800	BROWN	2%	C	SANDY	CLAY	
DS	-48	5	7	387	250	535	4795	BROWN	0%	C	SANDY	SOIL	
DS	-48	6	4	387	300	535	4790	BROWN	10%	C	SANDY	CLAY	
DS	-48	7	2	387	350	535	4800	BROWN	1%	C		CLAY	
DS	-48	8	6	387	400	535	4820	BROWN	0%	C	SANDY	SOIL	
DS	-48	9	7	387	450	535	4865	BLACK	0%	C	PEAT		
DS	-48	10	3	387	510	535	4810	BLACK	0%	C		CLAY	
DS	-48	11	1	387	550	535	4805	BROWN	0%	C	PEAT		
DS	-48	12	2	387	600	535	4780	BROWN	0%	C	SANDY	SOIL	
DS	-46	1	6	387	125	535	4675	BROWN	1%	C	SANDY	CLAY	deviation due to unmapped tarn
DS	-46	2	3	387	175	535	4710	BROWN	0%	C	PEAT		deviation due to unmapped tarn
DS	-46	3	5	387	225	535	4715	LIGHT BROWN	10%	C	SANDY	CLAY	deviation due to unmapped tarn
DS	-46	4	3	387	275	535	4675	BROWN	2%	C	PEAT		deviation due to unmapped tarn
DS	-46	5	3	387	325	535	4600	BROWN	0%	C		CLAY	
DS	-46	6	3	387	375	535	4600	BROWN	1%	C	PEAT		
DS	-46	7	2	387	425	535	4595	BROWN	0%	C	PEAT		
DS	-46	8	5	387	475	535	4595	BROWN	10%	C	PEAT		
DS	-46	9	1	387	525	535	4600	BROWN	15%	C	PEAT		
DS	-46	10	3	387	575	535	4570	BROWN	0%	C	PEAT		
DS	-46	11	5	387	625	535	4595	LIGHT BROWN	5%	C		CLAY	
DS	-46	12	3	387	675	535	4580	BROWN	2%	C	PEAT		deviation due to lake
DS	-46	13	3	387	725	535	4565	BROWN	0%	C	PEAT		deviation due to lake
DS	-46	14	4	387	775	535	4595	BROWN	2%	C		CLAY	
DS	-46	15	4	387	825	535	4600	BROWN	0%	C		CLAY	
DS	-46	16	5	387	875	535	4595	BROWN	10%	C		CLAY	

DS	-46	17	4	387	925	535	4600	BROWN	0%	C	PEAT		
DS	-46	18	3	387	975	535	4600	BROWN	0%	C	PEAT		
DS	-44	1	3	387	150	535	4425	LIGHT BROWN	10%	C	SANDY	CLAY	
DS	-44	2	1	387	200	535	4410	BROWN	0%	C	PEAT		
DS	-44	3	2	387	250	535	4400	BROWN	0%	C	PEAT		
DS	-44	4	1	387	300	535	4385	BROWN	10%	C		CLAY	
DS	-44	5	6	387	350	535	4370	BROWN	5%	C		CLAY	
DS	-44	6	2	387	400	535	4380	BROWN	10%	C		CLAY	
DS	-44	7	4	387	450	535	4405	BROWN	5%	C	SANDY	CLAY	
DS	-44	8	1	387	500	535	4405	BROWN	0%	C	SANDY	SOIL	
DS	-44	9	3	387	550	535	4405	BROWN	5%	C	SANDY	SOIL	
DS	-44	10	1	387	600	535	4410	BROWN	1%	C	PEAT		
DS	-44	11	1	387	650	535	4400	BROWN	10%	C		CLAY	
DS	-44	12	2	387	700	535	4395	BROWN	5%	C		CLAY	
DS	-44	13	2	387	750	535	4405	BROWN	5%	C		CLAY	
DS	-44	14	4	387	800	535	4400	BROWN	5%	C		CLAY	
DS	-44	15	1	387	850	535	4415	BROWN	10%	C		CLAY	
DS	-42	1	6	387	175	535	4200	DARK BROWN	1%	C	PEAT		
DS	-42	2	5	387	225	535	4200	BROWN	10%	C		CLAY	
DS	-42	3	6	387	275	535	4200	BROWN	10%	C		CLAY	
DS	-42	4	2	387	325	535	4200	BROWN	1%	C	SANDY	SOIL	
DS	-42	5	5	387	375	535	4200	BROWN	5%	C		CLAY	
DS	-42	6	1	387	425	535	4200	BROWN	5%	C		CLAY	
DS	-42	7	1	387	475	535	4285	LIGHT BROWN	0%	C	SANDY	SOIL	CONGLOMERATE BEDROCK
DS	-42	8	4	387	525	535	4245	BROWN	1%	C		CLAY	
DS	-42	9	3	387	575	535	4235	DARK BROWN	5%	C		CLAY	
DS	-42	10	2	387	625	535	4200	LIGHT BROWN	2%	C	SANDY	CLAY	
DS	-42	11	3	387	675	535	4200	LIGHT BROWN	1%	C	SANDY	CLAY	
DS	-42	12	3	387	725	535	4205	LIGHT BROWN	5%	C	SANDY	CLAY	
DS	-42	13	1	387	775	535	4210	BROWN	2%	C	PEAT		

DS	-42	14	1	387	825	535	4205	BROWN	5%	C	PEAT		
DS	-42	15	3	387	875	535	4200	BROWN	10%	C		CLAY	
DS	-42	16	4	387	925	535	4195	BROWN	5%	C		CLAY	
DS	-42	17	1	387	975	535	4200	BROWN	1%	C	PEAT		
DS	-40	1	1	387	300	535	4000	BROWN	0%	C	SANDY	GRAVEL	CONGLOMERATE BEDROCK
DS	-40	2	6	387	350	535	4000	BROWN	5%	C	PEAT		
DS	-40	3	1	387	400	535	4005	LIGHT BROWN	0%	C	SANDY	GRAVEL	CONGLOMERATE BEDROCK
DS	-40	4	4	387	450	535	4005	LIGHT BROWN	1%	C	SANDY	SOIL	
DS	-40	5	1	387	500	535	4005	BROWN	0%	C	PEAT		
DS	-40	6	1	387	550	535	4000	BROWN	15%	C		CLAY	
DS	-40	7	2	387	600	535	4000	BROWN	5%	C	SANDY	CLAY	
DS	-40	8	1	387	650	535	3995	BROWN	10%	C	PEAT		
DS	-40	9	3	387	700	535	4000	BROWN	5%	C	PEAT		
DS	-40	10	1	387	750	535	4000	BROWN	5%	C	PEAT		
DS	-40	11	3	387	800	535	4000	BROWN	10%	C	PEAT		
DS	-40	12	3	387	850	535	4000	BROWN	10%	C	PEAT		
DS	-40	13	1	387	900	535	4000	BROWN	20%	C	SANDY	GRAVEL	
DS	-40	14	5	387	950	535	4000	BROWN	1%	C	PEAT		
DS	-38	1	4	387	425	535	3795	BROWN	10%	C	SANDY	CLAY	
DS	-38	2	1	387	475	535	3800	BROWN	1%	C	PEAT		
DS	-38	3	4	387	525	535	3800	BROWN	10%	C		CLAY	
DS	-38	4	2	387	575	535	3800	BROWN	15%	C		CLAY	
DS	-38	5	2	387	625	535	3800	BROWN	10%	C	SANDY	CLAY	
DS	-38	6	4	387	675	535	3805	BROWN	15%	C		CLAY	
DS	-38	7	4	387	725	535	3800	GRAY	20%	C		CLAY	
DS	-38	8	3	387	775	535	3800	BROWN	10%	C	SANDY	CLAY	
DS	-38	9	3	387	825	535	3800	BROWN	10%	C	PEAT		
DS	-38	10	2	387	875	535	3795	DARK BROWN	2%	C	SANDY	CLAY	
DS	-38	11	3	387	925	535	3795	BROWN	2%	C	SANDY	SOIL	
DS	-38	12	2	387	975	535	3805	BROWN	1%	C	SANDY	CLAY	
DS	-38	13	3	388025		535	3805	LIGHT BROWN	20%	C	SANDY	CLAY	
DS	-38	14	1	388075		535	3805	BROWN	10%	C	PEAT		

DS	-38	15	2	388	125	535	3800	BROWN	5%	C	SANDY	CLAY	
DS	-38	16	4	388	175	535	3805	LIGHT BROWN	1%	C		CLAY	
DS	-36	1	1	387	500	535	3600	BROWN	2%	C	PEAT		
DS	-36	2	1	387	550	535	3605	BROWN	5%	C	PEAT		
DS	-36	3	4	387	600	535	3605	BROWN	2%	C	PEAT		
DS	-36	4	5	387	650	535	3605	BROWN	2%	C	PEAT		
DS	-36	5	4	387	700	535	3605	BROWN	1%	C	SANDY	SOIL	
DS	-36	6	3	387	750	535	3600	BROWN	2%	C	SANDY	SOIL	
DS	-36	7	4	387	800	535	3600	BROWN	0%	C		CLAY	
DS	-36	8	4	387	850	535	3600	YELLOWISH RED	15%	C		CLAY	
DS	-36	9	4	387	900	535	3605	GRAY	20%	C		CLAY	
DS	-36	10	1	387	950	535	3605	BROWN	0%	C		CLAY	
DS	-36	11	1	388000		535	3605	BROWN	1%	C	PEAT		
DS	-36	12	1	388050		535	3605	BROWN	0%	C	PEAT		
DS	-36	13	2	388	100	535	3605	BROWN	0%	C	PEAT		
DS	-36	14	3	388	145	535	3600	BROWN	0%	C	PEAT		
DS	-36	15	3	388	200	535	3615	BROWN	2%	C	SANDY	SOIL	
DS	-36	16	3	388	250	535	3600	LIGHT BROWN	2%	C		CLAY	
DS	-34	1	4	387	575	535	3415	LIGHT BROWN	0%	C	SANDY	SOIL	
DS	-34	2	2	387	625	535	3400	DARK BROWN	2%	C	PEAT		
DS	-34	3	1	387	675	535	3400	BROWN	1%	C	SANDY	SOIL	
DS	-34	4	4	387	725	535	3395	BROWN	5%	C	SANDY	SOIL	
DS	-34	5	3	387	775	535	3395	BROWN	4%	C		CLAY	
DS	-34	6	3	387	825	535	3400	BROWN	20%	C		CLAY	
DS	-34	7	4	387	875	535	3400	BROWN	5%	C		CLAY	
DS	-34	8	5	387	925	535	3405	BROWN	10%	C		CLAY	
DS	-34	9	4	387	975	535	3390	BROWN	2%	C		CLAY	
DS	-34	10	1	388025		535	3395	BROWN	0%	C	PEAT		
DS	-34	11	4	388075		535	3390	BROWN	10%	C		CLAY	
DS	-34	12	4	388	125	535	3400	BROWN	5%	C		CLAY	
DS	-34	13	1	388	175	535	3400	BROWN	0%	C	PEAT		
DS	-34	14	1	388	225	535	3380	BROWN	0%	C	PEAT		

DS	-34	15	1	388	275	535	3400	BROWN	10%	C	PEAT		
DS	-34	16	4	388	325	535	3400	BROWN	0%	C	PEAT		
DS	-32	1	1	387	600	535	3170	BROWN	2%	C	PEAT		
DS	-32	2	2	387	650	535	3175	BROWN	1%	C	PEAT		
DS	-32	3	2	387	700	535	3170	LIGHT BROWN	0%	C	SANDY	SOIL	
DS	-32	4	4	387	750	535	3150	GRAY	1%	C	SANDY	SOIL	
DS	-32	5	1	387	800	535	3150	BROWN	10%	C		CLAY	
DS	-32	6	1	387	850	535	3205	BROWN	20%	C	PEAT		
DS	-32	7	4	387	900	535	3215	BROWN	2%	C	PEAT		
DS	-32	8	4	387	950	535	3210	BROWN	4%	C		CLAY	
DS	-32	9	7	388000		535	3200	BROWN	10%	C		CLAY	
DS	-32	10	2	388050		535	3210	BROWN	1%	C	PEAT		
DS	-32	11	3	388	100	535	3205	BROWN	2%	C	SANDY	SOIL	
DS	-32	12	1	388	150	535	3210	LIGHT BROWN	10%	C	SANDY	SOIL	
DS	-32	13	2	388	200	535	3200	BROWN	1%	C	PEAT		
DS	-32	14	5	388	250	535	3200	BROWN	2%	C	C		
DS	-32	15	1	388	300	535	3205	BROWN	10%	C	SANDY	SOIL	
DS	-32	16	1	388	350	535	3205	BROWN	10%	C	PEAT		
DS	-32	17	2	388	400	535	3205	BROWN	5%	C	PEAT		
DS	-30	1	1	387	775	535	3020	BROWN	5%	C	PEAT		
DS	-30	2	1	387	825	535	3020	LIGHT BROWN	5%	C	PEAT		
DS	-30	3	3	387	875	535	3020	BROWN	5%	C		CLAY	
DS	-30	4	5	387	925	535	3015	BROWN	10%	C		CLAY	
DS	-30	5	1	387	975	535	3015	BROWN	5%	C	SANDY	SOIL	
DS	-30	6	6	388025		535	3020	BROWN	8%	C	SANDY	CLAY	
DS	-30	7	5	388075		535	3040	BROWN	10%	C		CLAY	
DS	-30	8	4	388	125	535	3015	LIGHT BROWN	20%	C		CLAY	
DS	-30	9	4	388	175	535	3005	BROWN	1%	C		CLAY	
DS	-30	10	5	388	225	535	3006	LIGHT BROWN	15%	C		CLAY	
DS	-30	11	3	388	275	535	3015	BROWN	10%	C		CLAY	
DS	-30	12	2	388	325	535	3005	GRAY	2%	C	SANDY	SOIL	
DS	-30	13	1	388	375	535	3020	BROWN	10%	C	PEAT		

DS	-30	14	4	388	425	535	3005	BROWN	10%	C	SANDY	SOIL	
DS	-30	15	4	388	475	535	2990	BROWN	10%	C		CLAY	
DS	-30	16	1	388	525	535	3000	BROWN	5%	C	PEAT		
DS	-28	1	1	387	805	535	2800	BROWN	2%	C	PEAT		
DS	-28	2	1	387	850	535	2810	BROWN	15%	C	PEAT		
DS	-28	3	1	387	900	535	2805	BROWN	10-%	C	PEAT		
DS	-28	4	4	387	950	535	2810	BROWN	5%	C		CLAY	
DS	-28	5	1	388000		535	2800	BROWN	10%	C	PEAT		
DS	-28	6	3	388050		535	2815	BROWN	10%	C	SANDY	SOIL	
DS	-28	7	1	388100		535	2820	BROWN	20%	C		CLAY	
DS	-28	8	3	388	150	535	2810	BROWN	10%	C		CLAY	
DS	-28	9	3	388	200	535	2805	BROWN	20%	C		CLAY	
DS	-28	10	5	388	250	535	2810	BROWN	5%	C		CLAY	
DS	-28	11	4	388	300	535	2800	BROWN	10%	C		CLAY	
DS	-28	12	4	388	350	535	2800	BROWN	10%	C		CLAY	
DS	-28	13	5	388	405	535	2805	BROWN	15%	C		CLAY	
DS	-28	14	4	388	450	535	2835	BROWN	10%	C		CLAY	
DS	-28	15	3	388	500	535	2805	BROWN	10%	C		CLAY	
RS	-80	1	6	386	175	535	8005	DARK BROWN	0%	C	PEAT		
RS	-80	2	3	386	225	535	8005	BROWN	0%	C	PEAT		
RS	-80	3	2	386	275	535	8010	DARK BROWN	0%	C	PEAT		
RS	-80	4	2	386	325	535	8000	BROWN	0%	C	PEAT		
RS	-80	5	3	386	375	535	8000	BROWN	0%	C	PEAT		
RS	-80	6	3	386	425	535	8000	DARK BROWN	0%	C	PEAT		
RS	-78	1	1	386	115	535	7805	BROWN	0%	A?	PEAT		ON CLIFF FACE
RS	-78	2	4	386	150	535	7805	LIGHT BROWN	0%	C	PEAT		
RS	-78	3	5	386	200	535	7800	LIGHT BROWN	10%	C	PEAT		
RS	-78	4	4	386	250	535	7800	BROWN	10%	C	PEAT		
RS	-78	5	8	386	300	535	7800	DARK BROWN	1%	C	PEAT		
RS	-78	6	6	386	350	535	7800	BROWN	10%	C	PEAT		
RS	-78	7	3	386	400	535	7800	BROWN	5%	C	PEAT		

RS	-78	8	6	386	450	535	7810	BROWN	0%	C	PEAT		
RS	-78	9	5	386	500	535	7805	LIGHT BROWN	5%	C	PEAT		
RS	-76	1	7	386	225	535	7600	GRAYISH BROWN	2%	C	PEAT		
RS	-76	2	4	386	275	535	7605	GRAYISH BROWN	2%	C	PEAT		
RS	-76	3	5	386	325	535	7600	DARK BROWN	0%	C	SOIL		
RS	-76	4	3	386	375	535	7610	GRAY	2%	C	PEAT		
RS	-76	5	2	386	425	535	7600	DARK BROWN	0%	C	SOIL		
RS	-76	6	1	386	475	535	7610	BROWN	0%	C	SOIL		
RS	-76	7	2	386	525	535	7605	BROWN	0%	C	SOIL		
RS	-76	8	4	386	575	535	7600	DARK BROWN	0%	C	SOIL		
RS	-76	9	2	386	175	535	7600	GRAY	2%	C	PEAT		
RS	-74	1	1	386	251	535	7415	GRAY	5%	C	PEAT		
RS	-74	2	2	386	300	535	7400	BROWN	0%	C	PEAT		
RS	-74	3	1	386	350	535	7405	GRAY	2%	C	PEAT		
RS	-74	4	1	386	410	535	7400	BROWN	0%	C	PEAT		
RS	-74	5	1	386	460	535	7380	GRAY	0%	C	PEAT		
RS	-74	6	1	386	500	535	7400	GRAY	0%	C	PEAT		
RS	-74	7	2	386	555	535	7400	BROWN	0%	C	PEAT		
RS	-74	8	2	386	600	535	7400	BROWN	0%	C	PEAT		
RS	-72	1	2	386	325	535	7200	LIGHT BROWN	0%	C	PEAT		
RS	-72	2	2	386	375	535	7215	GRAY	0%	C	PEAT		
RS	-72	3	2	386	425	535	7205	GRAY	0%	C	PEAT		
RS	-72	4	3	386	475	535	7200	GRAY	0%	C	PEAT		
RS	-72	5	1	386	530	535	7195	GRAY	0%	C		CLAY	
RS	-72	6	1	386	575	535	7200	LIGHT BROWN	0%	C	PEAT		
RS	-72	7	5	386	625	535	7200	GRAY	20%	C		CLAY	
RS	-72	8	1	386	675	535	7200	BROWN	0%	C	PEAT		
RS	-72	9	6	386	725	535	7200	BROWN	6%	C		CLAY	

RS	-72	10	3	386	775	535	7195	BROWN	2%	C	PEAT		
RS	-70	1	2	386	400	535	7000	BROWN	0%	C	PEAT		
RS	-70	2	1	386	450	535	7005	GRAY	2%	C	PEAT		
RS	-70	3	2	386	500	535	7000	GRAY	0%	C	PEAT		
RS	-70	4	5	386	551	535	7000	GRAY	2%	C	PEAT		
RS	-70	5	2	386	600	535	7015	BROWN	0%	C		CLAY	
RS	-70	6	3	386	650	535	7020	GRAY	2%	C		CLAY	
RS	-70	7	3	386	700	535	7030	GRAY	0%	C		CLAY	
RS	-70	8	3	386	750	535	7030	BROWN	5%	C		CLAY	
RS	-70	9	5	386	800	535	7040	BROWN	5%	C		CLAY	
RS	-70	10	4	386	850	535	7000	BROWN	5%	C		CLAY	
RS	-68	1	2	386	425	535	6800	BROWN	1%	C	PEAT		
RS	-68	2	2	386	475	535	6800	GRAY	5%	C	PEAT		
RS	-68	3	2	386	525	535	6805	GRAY	2%	C	PEAT		
RS	-68	4	1	386	575	535	6800	GRAY	1%	C	PEAT		
RS	-68	5	3	386	625	535	6800	GRAY	1%	C		SOIL	VERY WET
RS	-68	6	5	386	675	535	6800	GRAY	1%	C	PEAT		
RS	-68	7	2	386	725	535	6795	GRAY	1%	C	PEAT		
RS	-68	8	3	386	775	535	6805	GRAY	1%	C	PEAT		
RS	-68	9	4	386	825	535	6800	GRAY	1%	C		SOIL	SANDY TOP SOIL
RS	-68	10	5	386	875	535	6800	GRAY	1%	C	PEAT		
RS	-68	11	5	386	925	535	6800	GRAY	1%	C	PEAT		
RS	-68	12	5	386	975	535	6795	GRAY	1%	C	PEAT		
RS	-68	13	4	387025		535	6800	BROWN	5%	A?		SOIL	
RS	-68	14	4	387075		535	6800	GRAY	5%	C	PEAT		
RS	-68	15	4	387	125	535	6800	GRAY	10%	C	CLAY		
RS	-66	1	3	386	450	535	6605	GRAY	10%	C		GRAVEL	WET
RS	-66	2	7	386	500	535	6605	BROWN	0%	C	PEAT &	GRAVEL	WET
RS	-66	3	2	386	550	535	6600	GRAY	2%	C		GRAVEL	
RS	-66	4	3	386	600	535	6600	GRAY	0%	C		GRAVEL	
RS	-66	5	4	386	650	535	6610	GRAY	0%	C	SOIL &	GRAVEL	
RS	-66	6	3	386	700	535	6600	GRAY	2%	C	SOIL &	GRAVEL	
RS	-66	7	3	386	750	535	6600	BROWN	0%	C	TILL		
RS	-66	8	2	386	800	535	6615	BROWN	2%	C	TILL		
RS	-66	9	4	386	850	535	6610	BROWN	1%	C	TILL		
RS	-66	10	3	386	900	535	6625	BROWN	4%	C	TILL		

RS	-66	11	3	386	950	535	6640	BROWN	10%	C	TILL		
RS	-66	12	4	387000		535	6610	BROWN	2%	C	SANDY	SOIL	
RS	-66	13	5	387050		535	6605	LIGHT BROWN	5%	C	SANDY	SOIL	
RS	-66	14	4	387	100	535	6610	GRAYISH BROWN	5%	C	SANDY	SOIL	
RS	-66	15	3	387	150	535	6610	GRAY	2%	C	SANDY	SOIL	
RS	-66	16	4	387	200	535	6605	GRAY	2%	C	SANDY	SOIL	
RS	-66	17	6	387	250	535	6600	GRAY	2%	C	SANDY	SOIL	
RS	-64	1	1	386	475	535	6395	GRAY	2%	C	SANDY	CLAY	ON BEDROCK
RS	-64	2	5	386	525	535	6395	BROWN	5%	C	SANDY	SOIL	
RS	-64	3	4	386	575	535	6390	GRAY	5%	C	SANDY	CLAY	
RS	-64	4	6	386	625	535	6400	BROWN	2%	C	SANDY	SOIL	
RS	-64	5	4	386	675	535	6400	BROWN	5%	C	SANDY	SOIL	
RS	-64	6	3	386	725	535	6405	BROWN	2%	C	SANDY	SOIL	
RS	-64	7	3	386	775	535	6400	BROWN	0%	C	SANDY	CLAY	
RS	-64	8	4	386	825	535	6395	LIGHT BROWN	2%	C	SANDY	CLAY	
RS	-64	9	4	386	875	535	6400	LIGHT BROWN	5%	C	SANDY	CLAY	
RS	-64	10	2	386	925	535	6405	LIGHT BROWN	1%	C	SANDY	CLAY	
RS	-64	11	4	386	975	535	6410	LIGHT BROWN	5%	C	SANDY	PEAT	
RS	-64	12	4	387025		535	6430	GRAY	0%	C		CLAY	
RS	-64	13	3	387075		535	6420	GRAY	2%	C	SANDY	CLAY	
RS	-64	14	3	387	125	535	6430	GRAY	5%	C	SANDY	CLAY	
RS	-64	15	3	387	175	535	6430	GRAY	5%	C	SANDY	CLAY	
RS	-64	16	2	387	225	535	6430	BROWN	0%	C	PEAT		
RS	-64	17	3	387	275	535	6430	LIGHT BROWN	5%	C	SANDY	PEAT	
RS	-64	18	4	387	325	535	6425	LIGHT BROWN	5%	C	SANDY	PEAT	
RS	-64	19	2	387	375	535	6425	BROWN	2%	C	SANDY	PEAT	
RS	-62	1	2	386	605	535	6205	BROWN	0%	C	SANDY	SOIL	
RS	-62	2	3	386	650	535	6200	BROWN	0%	C	SANDY	SOIL	
RS	-62	3	2	386	700	535	6190	LIGHT	0%	C	PEAT		

								BROWN					
RS	-62	4	3	386	750	535	6180	LIGHT BROWN	0%	C		GRAVEL	
RS	-62	5	4	386	800	535	6200	LIGHT BROWN	0%	C		GRAVEL	
RS	-62	6	3	386	850	535	6200	LIGHT BROWN	0%	C	PEAT		
RS	-62	7	3	386	900	535	6200	LIGHT BROWN	0%	C	SANDY	SOIL	
RS	-62	8	4	386	950	535	6195	LIGHT BROWN	0%	C	PEAT		
RS	-62	9	6	387000		535	6200	LIGHT BROWN	0%	C	SANDY	CLAY	
RS	-62	10	5	387050		535	6195	LIGHT BROWN	0%	C	SANDY	CLAY	
RS	-62	11	3	387	100	####		LIGHT BROWN	10%	C	SANDY	SOIL	
RS	-62	12	1	387	150	####		LIGHT BROWN	2%	C	SANDY	SOIL	
RS	-62	13	4	387	200	535	6190	LIGHT BROWN	0%	C	PEAT		
RS	-62	14	2	387	250	535	6190	BROWN	10%	C	PEAT		
RS	-62	15	3	387	300	535	6190	BROWN	2%	C	PEAT		
RS	-62	16	2	387	350	535	6195	BROWN	1%	C	PEAT		
RS	-62	17	2	387	400	535	6200	BROWN	0%	C	PEAT		
RS	-62	18	3	387	450	535	6200	BROWN	0%	C	PEAT		
RS	-60	1	4	386	825	535	6000	LIGHT BROWN	5%	C	SANDY	SOIL	
RS	-60	2	4	386	875	535	5990	LIGHT BROWN	10%	C		CLAY	
RS	-60	3	1	386	925	535	5990	BROWN	0%	?	PEAT		PEAT ON BEDROCK
RS	-60	4	4	386	975	535	5990	BROWN	5%	C	SANDY	CLAY	
RS	-60	5	2	387025		535	5995	BROWN	5%	C	SANDY	CLAY	
RS	-60	6	4	387075		535	5995	GRAY	0%	C	SANDY	CLAY	
RS	-60	7	3	387	125	535	5995	BROWN	0%	C	SANDY	CLAY	
RS	-60	8	4	387	175	535	5995	BROWN	0%	C	SANDY	CLAY	
RS	-60	9	5	387	225	535	6005	BROWN	2%	C	SANDY	CLAY	

RS	-60	10	5	387	275	535	6015	BROWN	4%	C		CLAY	
RS	-60	11	3	387	325	535	6005	BROWN	6%	C	SANDY	SOIL	
RS	-60	12	3	387	375	535	6005	BROWN	2%	C	SANDY	SOIL	
RS	-60	13	2	387	425	535	6010	BROWN	0%	C	SANDY	SOIL	
RS	-60	14	4	387	475	535	6010	BROWN	5%	C	PEAT		
RS	-60	15	5	387	525	535	6010	BROWN	2%	C	PEAT		
RS	-60	16	4	387	570	535	6000	BROWN	4%	C	SANDY	CLAY	
RS	-58	1	7	386	700	535	5805	GRAY	0%	C		CLAY	
RS	-58	2	1	386	750	535	5800	GRAY	0%	C	PEAT		
RS	-58	3	4	386	800	535	5800	GRAY	5%	C	SANDY	CLAY	
RS	-58	4	3	386	850	535	5800	BROWN	2%	C	SANDY	CLAY	
RS	-58	5	1	386	900	535	5810	BROWN	0%	C	SANDY	PEAT	
RS	-58	6	3	386	950	535	5805	BROWN	2%	C	SANDY	PEAT	
RS	-58	7	4	387000		535	5800	BROWN	5%	C	SANDY	PEAT	
RS	-58	8	1	387050		535	5795	BROWN	1%	C	PEAT		
RS	-58	9	6	387	100	535	5790	BROWN	2%	C	PEAT		
RS	-58	10	3	387	150	535	5795	BROWN	0%	C	PEAT		
RS	-58	11	1	387	200	535	5790	BROWN	1%	C	PEAT		
RS	-58	12	5	387	250	535	5800	BROWN	2%	C	PEAT &	CLAY	
RS	-58	13	2	387	300	535	5800	BROWN	10%	C	PEAT &	CLAY	
RS	-58	14	2	387	350	535	5800	BROWN	0%	C	PEAT &	CLAY	
RS	-58	15	4	387	400	535	5805	BROWN	5%	C	PEAT		
RS	-58	16	4	387	450	535	5800	LIGHT BROWN	2%	C	SANDY	CLAY	
RS	-58	17	4	387	500	535	5800	BROWN	5%	C		CLAY	
RS	-58	18	6	387	550	535	5800	BROWN	5%	C	SANDY	CLAY	
RS	-58	19	5	387	600	535	5800	BROWN	5%	C	SANDY	CLAY	
RS	-58	20	6	387	650	535	5800	BROWN	10%	C	SANDY	CLAY	
RS	-58	21	12	387	700	535	5805	DARK BROWN	1%	A?	MARSHY	SOIL	NO B OR C HOR. FOR 30M
RS	-56	1	4	386	625	535	5600	BROWN	0%	C	SANDY	CLAY	
RS	-56	2	1	386	675	535	5580	BROWN	0%	C	PEAT		
RS	-56	3	1	386	725	535	5590	GRAY	0%	C	SANDY	PEAT	
RS	-56	4	4	386	775	535	5600	GRAY	8%	C	SANDY	CLAY	
RS	-56	5	5	386	825	535	5600	BROWN	0%	C	SANDY	CLAY	
RS	-56	6	4	386	875	535	5600	BROWN	0%	C	SANDY	CLAY	

RS	-54	1	5	386	550	535	5420	GRAY	4%	C	SANDY	SOIL	
RS	-54	2	3	386	600	535	5410	GRAY	0%	C	SANDY	CLAY	
RS	-54	3	5	386	650	535	5405	LIGHT BROWN	2%	C	SANDY	CLAY	
RS	-54	4	6	386	700	535	5400	LIGHT BROWN	1%	C		CLAY	
RS	-54	5	1	386	750	535	5395	LIGHT BROWN	0%	C	PEAT		
RS	-54	6	5	386	800	535	5410	LIGHT BROWN	1%	C	CLAYEY	SOIL	

APPENDIX 2

(Six Monthly Report)

Soil Geochemical Sample Assays

Sample_no	Northing	Easting	Au_ppb	Au-Rp1	Ag_ppm	As_ppm	Bi_ppm	Cu_ppm	Mo_ppm	Pb_ppm	Sb_ppm	Tl_ppm	Zn_ppm
DS-4801	5354790	387050	1		0.02	0.6	0.03	6	0.5	3	0.15	0.05	6
DS-4802	5354800	387100	1		0.02	1.4	0.16	11	0.8	13	0.29	0.04	6
DS-4803	5354810	387150	0.1		0.03	0.05	0.11	6	0.5	17	0.24	0.14	15
DS-4804	5354800	387200	0.1		0.02	0.8	0.07	9	0.7	13	0.22	0.08	10
DS-4805	5354795	387250	0.1		0.03	0.05	0.09	7	0.5	14	0.15	0.06	7
DS-4806	5354790	387300	0.1		0.02	1.3	0.09	8	0.7	10	0.12	0.04	7
DS-4807	5354800	387350	0.1		0.01	0.05	0.05	7	0.5	5	0.1	0.05	5
DS-4808	5354820	387400	1		0.02	0.7	0.07	8	0.6	9	0.12	0.05	10
DS-4809	5354865	387450	0.1		0.02	1	0.03	9	0.9	10	0.11	0.03	6
DS-4810	5354810	387510	0.1		0.03	0.6	0.05	8	0.7	8	0.13	0.05	9
DS-4811	5354805	387550	0.1		0.03	3.4	0.47	15	0.9	48	0.53	0.11	14
DS-4812	5354780	387600	1		0.03	1.1	0.2	11	0.9	21	0.21	0.06	12
DS-4601	5354675	387125	0.1		0.08	0.5	0.08	8	0.7	31	0.25	0.09	9
DS-4602	5354710	387175	0.1		0.07	5.7	0.35	14	1	40	0.24	0.18	17
DS-4603	5354715	387225	0.1		0.04	1.3	0.19	8	0.6	34	0.18	0.13	13
DS-4604	5354675	387275	0.1		0.02	1.6	0.18	10	0.8	19	0.2	0.06	12
DS-4605	5354600	387325	0.1		0.02	1.6	0.26	10	0.6	22	0.14	0.09	13
DS-4606	5354600	387375	4		0.01	1.2	0.06	7	0.7	8	0.12	0.1	9
DS-4607	5354595	387425	0.1		0.01	0.8	0.05	5	0.6	9	0.08	0.06	8
DS-4608	5354595	387475	0.1		0.02	1.8	0.26	9	0.6	22	0.1	0.08	14
DS-4609	5354600	387525	0.1		0.04	3.4	1.33	39	0.8	73	0.23	0.18	12
DS-4610	5354570	387575	18		0.08	3.1	3.69	38	0.8	49	0.18	0.14	16
DS-4611	5354595	387625	4		0.08	0.7	2.36	11	0.4	20	0.07	0.12	12
DS-4612	5354580	387675	178	175	0.11	2.4	1.43	12	0.6	66	0.19	0.1	40
DS-4613	5354565	387725	9		0.07	3.2	0.59	9	0.6	45	0.24	0.1	22
DS-4614	5354595	387775	5		0.1	1	0.33	6	0.4	42	0.44	0.44	37
DS-4615	5354600	387825	5		0.06	0.6	0.33	8	0.6	27	0.12	0.13	16
DS-4616	5354595	387875	2		0.04	1.6	0.65	11	0.4	48	0.2	0.12	11
DS-4617	5354600	387925	5		0.02	1.2	0.54	9	0.4	29	0.12	0.09	13
DS-4618	5354600	387975	13		0.03	0.7	0.12	7	0.4	11	0.07	0.04	12
DS-4401	5354425	387150	0.1		0.02	2.7	0.07	8	0.8	18	0.5	0.12	10

DS-4402	5354410	387200	17		0.01	1.6	0.24	16	1.2	19	0.46	0.1	17
DS-4403	5354400	387250	1		0.001	0.6	0.05	10	0.8	71	0.24	0.03	9
DS-4404	5354385	387300	1		0.001	1.4	0.12	8	0.8	21	0.15	0.03	5
DS-4405	5354370	387350	0.1		0.001	0.05	0.02	7	0.6	4	0.12	0.04	5
DS-4406	5354380	387400	0.1		0.001	0.8	0.11	8	0.9	13	0.15	0.03	10
DS-4407	5354405	387450	2		0.06	3.3	0.52	16	1.6	38	0.18	0.09	20
DS-4408	5354405	387500	0.1		0.05	1.3	0.44	13	1.1	41	0.25	0.06	14
DS-4409	5354405	387550	111	80	0.17	1.3	5.41	77	0.9	68	0.06	0.07	34
DS-4410	5354410	387600	3		0.08	3.7	0.7	85	1.6	59	0.38	0.12	21
DS-4411	5354400	387650	2		0.03	1	0.47	8	0.6	30	0.13	0.09	31
DS-4412	5354395	387700	3		0.05	2.3	0.44	16	1	65	0.33	0.12	43
DS-4413	5354405	387750	3		0.09	2.4	0.4	11	0.9	42	0.32	0.15	30
DS-4414	5354400	387800	15		0.1	1.2	0.38	10	0.9	74	0.23	0.11	40
DS-4415	5354415	387850	2		0.11	5.3	1.55	22	0.6	126	0.81	0.31	28
DS-4201	5354200	387175	2		0.02	1.1	0.14	10	1	7	0.15	0.03	5
DS-4202	5354200	387225	1		0.01	0.05	0.01	6	0.6	3	0.06	0.02	4
DS-4203	5354200	387275	0.1		0.001	0.05	0.04	10	1	5	0.15	0.09	4
DS-4204	5354200	387325	0.1		0.001	0.05	0.16	10	1	16	0.18	0.02	4
DS-4205	5354200	387375	3		0.14	0.9	0.08	8	1	10	0.14	0.16	6
DS-4206	5354200	387425	11		0.11	2.8	0.43	16	1	104	0.31	0.16	77
DS-4207	5354285	387475	5		0.04	0.8	0.36	15	1.1	31	0.26	0.07	9
DS-4208	5354245	387525	2		0.37	1.3	0.32	9	0.9	88	0.18	0.1	70
DS-4209	5354235	387575	2		0.13	1.6	0.35	12	0.8	153	0.24	0.09	61
DS-4210	5354200	387625	11		0.09	1.6	0.36	12	1.1	37	0.34	0.12	16
DS-4211	5354200	387675	0.1		0.06	1.5	0.43	10	0.7	43	0.25	0.1	28
DS-4212	5354205	387725	0.1		0.04	0.6	0.17	8	0.8	34	0.14	0.04	20
DS-4213	5354210	387775	0.1		0.08	2.1	0.56	22	0.7	64	0.61	0.2	27
DS-4214	5354205	387825	1		0.05	1	0.38	13	0.9	39	0.21	0.05	16
DS-4215	5354200	387875	2		0.06	1.6	0.29	11	0.7	42	0.19	0.08	21
DS-4216	5354195	387925	0.1		0.04	1.2	0.25	7	0.6	55	0.23	0.13	21
DS-4217	5354200	387975	0.1		0.06	2.1	0.51	20	1.4	55	0.4	0.11	15
DS-4001	5354000	387300	1		0.001	0.05	0.11	9	1.1	9	0.13	0.02	5

DS-4002	5354000	387350	0.1		0.001	0.05	0.03	7	0.8	2	0.1	0.03	14
DS-4003	5354005	387400	0.1		0.001	0.5	0.16	9	1.3	12	0.18	0.02	5
DS-4004	5354005	387450	2		0.001	0.6	0.05	7	0.8	9	0.1	0.04	6
DS-4005	5354005	387500	1		0.01	6.4	0.95	18	1.3	67	0.57	0.11	8
DS-4006	5354000	387550	0.1		0.001	1.5	0.12	8	0.9	19	0.23	0.08	6
DS-4007	5354000	387600	3		0.001	2	0.26	12	1.1	33	0.41	0.2	101
DS-4008	5353995	387650	2		0.01	1	0.35	12	1.1	40	0.22	0.07	32
DS-4009	5354000	387700	2		0.41	2.2	1.42	20	1.2	142	0.24	0.18	66
DS-4010	5354000	387750	4		0.17	1.7	0.31	14	1	57	0.17	0.05	32
DS-4011	5354000	387800	10		0.09	1.9	0.21	11	0.9	38	0.17	0.07	15
DS-4012	5354000	387850	6		0.09	1.1	0.14	8	0.8	32	0.17	0.11	23
DS-4013	5354000	387900	3		0.15	4.8	1.19	42	1.4	145	0.76	0.21	25
DS-4014	5354000	387950	3		0.04	1.5	0.07	7	1.1	11	0.14	0.04	8
DS-3801	5353795	387425	1		0.04	2.9	0.1	9	0.7	7	0.31	0.03	2
DS-3802	5353800	387475	3		0.02	1.4	0.21	10	0.6	17	0.37	0.04	8
DS-3803	5353800	387525	0.1		0.01	1.6	0.1	6	0.4	11	0.68	0.46	11
DS-3804	5353800	387575	3		0.03	1.7	0.1	9	0.4	11	0.27	0.12	6
DS-3805	5353800	387625	1		0.02	2.3	0.19	13	0.6	28	0.37	0.15	10
DS-3806	5353805	387675	3		0.09	2.3	0.15	7	0.4	74	0.62	0.19	29
DS-3807	5353800	387725	4		0.04	1.2	0.43	10	0.8	56	0.3	0.15	29
DS-3808	5353800	387775	0.1		0.04	1.3	0.29	11	0.8	35	0.14	0.05	17
DS-3809	5353800	387825	3		0.06	1.9	0.5	16	1.1	42	0.29	0.05	41
DS-3810	5353795	387875	0.1		0.03	1.8	0.3	10	0.9	38	0.27	0.12	34
DS-3811	5353795	387925	4		0.04	1	0.32	12	1.2	28	0.51	0.08	39
DS-3812	5353805	387975	1		0.05	2.1	0.73	22	1.2	84	0.49	0.09	41
DS-3813	5353805	388025	3		0.09	2.3	0.97	33	1	90	0.44	0.17	65
DS-3814	5353805	388075	5		0.04	3.5	0.64	22	1.7	70	0.53	0.14	25
DS-3815	5353800	388125	1		0.04	5.1	0.7	18	0.8	45	0.74	0.19	26
DS-3816	5353805	388175	2		0.03	3	0.39	13	0.7	32	0.42	0.16	25
DS-3601	5353600	387500	3		0.02	2.4	0.39	12	0.3	35	0.39	0.04	3
DS-3602	5353605	387550	1		0.01	2.8	0.2	9	0.4	20	0.67	0.29	14
DS-3603	5353605	387600	2		0.02	4.1	0.39	11	0.5	35	0.94	0.3	19

DS-3604	5353605	387650	0.1		0.01	1.6	0.07	8	0.4	7	0.29	0.08	8
DS-3605	5353605	387700	2		0.02	4.3	0.43	14	0.5	48	2.6	0.36	232
DS-3606	5353600	387750	2		0.04	3.2	0.26	13	0.6	148	2.77	0.18	34
DS-3607	5353600	387800	4		0.04	2.3	0.26	11	0.4	106	0.86	0.29	32
DS-3608	5353600	387850	2		0.19	2.4	1.62	9	0.4	73	0.49	0.35	74
DS-3609	5353605	387900	5		0.4	2.9	3.85	32	0.6	194	0.47	0.21	85
DS-3610	5353605	387950	2		0.13	7.3	0.84	18	0.7	131	0.51	0.26	39
DS-3611	5353605	388000	4		0.2	4.4	2.18	27	0.9	109	1.56	0.37	15
DS-3612	5353605	388050	4		0.11	2.4	0.5	16	0.5	45	0.57	0.18	22
DS-3613	5353605	388100	1		0.08	2.2	0.97	26	0.7	80	0.81	0.14	21
DS-3614	5353600	388145	2		0.05	2.4	0.53	16	0.3	61	0.54	0.11	31
DS-3615	5353615	388200	0.1		0.07	3	0.62	15	0.7	37	0.94	0.1	18
DS-3616	5353600	388250	4		0.14	1.3	0.14	6	0.4	14	0.3	0.06	18
DS-3401	5353415	387575	4		0.001	0.7	0.14	11	0.4	14	0.16	0.06	3
DS-3402	5353400	387625	6		0.03	4.4	0.4	12	0.8	25	0.56	0.22	20
DS-3403	5353400	387675	5		0.04	4.5	2.22	37	0.9	183	1.62	0.51	20
DS-3404	5353395	387725	3		0.02	2	0.16	7	0.3	12	0.71	0.37	12
DS-3405	5353395	387775	1		0.02	9.9	0.17	11	0.8	13	8.58	0.67	29
DS-3406	5353400	387825	8		0.01	1.2	0.15	8	0.3	28	0.53	0.15	23
DS-3407	5353400	387875	3		0.02	1.4	0.17	9	0.6	42	0.43	0.22	16
DS-3408	5353405	387925	3		0.03	1.3	0.35	9	0.7	40	0.34	0.19	19
DS-3409	5353390	387975	21		0.05	1.9	0.34	9	0.6	99	1.15	0.35	37
DS-3410	5353395	388025	2		0.31	4.7	1.51	51	1.9	815	0.6	0.15	63
DS-3411	5353390	388075	3		0.15	2.8	1.04	24	0.3	167	0.91	0.34	29
DS-3412	5353400	388125	5		0.06	1.8	0.25	11	0.3	51	0.36	0.13	26
DS-3413	5353400	388175	2		0.06	3.9	1.51	37	0.5	135	1.36	0.35	55
DS-3414	5353380	388225	4		0.06	10.9	3.89	54	0.5	267	1.94	0.51	33
DS-3415	5353400	388275	0.1		0.04	2.2	0.3	11	0.4	27	0.45	0.16	14
DS-3416	5353400	388325	0.1		0.02	1.4	0.12	8	0.2	10	0.2	0.09	7
DS-3201	5353170	387600	1		0.07	5.2	1.4	49	1.1	146	1.14	0.21	30
DS-3202	5353175	387650	2		0.09	2.1	0.8	26	0.8	91	1.14	0.19	41
DS-3203	5353170	387700	1		0.07	2.9	1.01	40	1	94	1.04	0.25	20

DS-3204	5353150	387750	1		0.07	1.4	0.71	21	1.1	55	0.79	0.33	18
DS-3205	5353150	387800	4		0.04	1	0.15	10	0.7	16	0.14	0.05	3
DS-3206	5353205	387850	6		0.24	4.6	4.77	94	1.2	407	3.12	0.62	30
DS-3207	5353215	387900	1		0.11	2.1	0.88	28	1.1	75	1.43	0.5	28
DS-3208	5353210	387950	3		0.2	4.1	0.34	12	0.7	67	0.7	0.23	34
DS-3209	5353200	388000	9		0.11	1.2	0.33	11	0.8	66	0.63	0.22	21
DS-3210	5353210	388050	5		0.06	0.7	0.06	13	1	23	0.28	0.1	13
DS-3211	5353205	388100	3		0.07	6.4	0.79	22	0.8	121	0.84	0.42	63
DS-3212	5353210	388150	4		0.04	1.2	0.17	9	0.7	31	0.32	0.14	26
DS-3213	5353200	388200	3		0.06	5.2	1.51	44	1	82	0.86	0.25	22
DS-3214	5353200	388250	0.1		0.05	2.3	0.87	19	0.9	47	1.08	0.25	42
DS-3215	5353205	388300	2		0.04	2.4	0.37	16	0.9	46	0.49	0.17	15
DS-3216	5353205	388350	0.1		0.03	4.2	0.54	16	0.5	29	0.5	0.15	8
DS-3217	5353205	388400	0.1		0.02	1	0.16	9	0.7	11	0.19	0.06	8
DS-3001	5353020	387775	3		0.01	1	0.34	18	0.9	30	0.26	0.02	5
DS-3002	5353020	387825	11		0.08	3.8	1.6	27	1	87	3.42	0.56	17
DS-3003	5353020	387875	6		0.06	1.7	0.54	26	1.8	51	0.54	0.15	11
DS-3004	5353015	387925	6		0.03	1.5	0.24	14	0.2	27	0.34	0.24	13
DS-3005	5353015	387975	4		0.04	3.3	0.85	33	0.6	72	0.9	0.34	18
DS-3006	5353020	388025	4		0.03	2.7	0.49	14	0.3	35	0.62	0.24	15
DS-3007	5353040	388075	4		0.02	1.5	0.13	7	0.5	11	0.33	0.09	11
DS-3008	5353015	388125	3		0.02	0.8	0.17	6	0.4	13	0.32	0.13	10
DS-3009	5353005	388175	7		0.02	0.05	0.07	5	0.1	32	0.26	0.14	11
DS-3010	5353006	388225	2		0.01	2.8	0.32	9	0.3	29	0.33	0.1	11
DS-3011	5353015	388275	3		0.01	0.9	0.19	8	0.5	28	0.46	0.15	19
DS-3012	5353005	388325	8		0.01	1	0.25	14	0.8	17	0.24	0.05	13
DS-3013	5353020	388375	1		0.05	2.9	0.95	42	3.6	80	0.72	0.09	14
DS-3014	5353005	388425	6		0.02	1.7	0.13	10	0.8	16	0.29	0.08	21
DS-3015	5352990	388475	2		0.04	1.5	0.19	13	0.5	32	0.23	0.1	15
DS-3016	5353000	388525	0.1		0.05	1.1	0.07	9	0.5	8	0.15	0.06	7
DS-2801	5352800	387805	4		0.08	2.7	0.72	39	1.3	73	0.68	0.05	18
DS-2802	5352810	387850	2		0.04	1.1	0.62	17	0.7	46	0.43	0.11	4

DS-2803	5352805	387900	4		0.01	1.3	0.29	15	0.01	24	0.2	0.05	2
DS-2804	5352810	387950	3		0.02	3.1	0.39	15	0.6	28	0.66	0.19	13
DS-2805	5352800	388000	6		0.04	1.2	0.11	13	0.4	9	0.37	0.13	7
DS-2806	5352815	388050	2		0.04	1.6	0.18	10	0.2	10	0.26	0.09	5
DS-2807	5352820	388100	2		0.05	1.9	0.5	19	0.8	36	0.49	0.11	8
DS-2808	5352810	388150	6		0.02	2.2	0.27	13	0.5	22	0.24	0.05	6
DS-2809	5352805	388200	2		0.03	1.5	0.69	24	0.6	47	0.44	0.2	10
DS-2810	5352810	388250	2		0.01	1.1	0.18	12	0.7	20	0.28	0.14	14
DS-2811	5352800	388300	0.1		0.05	0.9	0.08	10	0.6	10	0.33	0.11	10
DS-2812	5352800	388350	1		0.03	1.2	0.18	10	0.6	32	0.28	0.13	13
DS-2813	5352805	388405	5		0.02	0.8	0.08	8	0.5	15	0.16	0.08	11
DS-2814	5352835	388450	2		0.001	1.1	0.1	8	0.4	9	0.08	0.07	8
DS-2815	5352805	388500	0.1		0.001	1.3	0.51	19	0.5	54	0.2	0.1	6
RS-8001	5358005	386175	0.1		0.04	0.6	0.84	11	1.1	6	0.09	0.03	5
RS-8002	5358005	386225	0.1		0.04	0.6	0.33	10	1.2	10	0.06	0.03	3
RS-8003	5358010	386275	0.1		0.03	0.05	0.35	11	0.9	3	0.07	0.02	3
RS-8004	5358000	386325	2		0.1	1.7	0.36	14	1.8	30	0.39	0.17	13
RS-8005	5358000	386375	1		0.12	0.5	0.15	11	1.1	14	0.23	0.09	17
RS-8006	5358000	386425	0.1		0.08	1	0.97	13	1.7	20	0.25	0.1	20
RS-7801	5357805	386115	0.1		0.09	0.05	1.81	55	1.1	208	0.68	0.03	27
RS-7802	5357805	386150	0.1		0.12	0.6	1.73	6	0.5	17	0.34	0.12	10
RS-7803	5357800	386200	0.1		0.06	0.6	2.78	8	0.6	12	0.32	0.11	8
RS-7804	5357800	386250	0.1		0.09	0.8	0.97	9	1.2	10	0.41	0.1	9
RS-7805	5357800	386300	0.1		0.14	0.9	1.58	13	2.1	19	0.29	0.12	26
RS-7806	5357800	386350	0.1		0.11	0.8	2.65	9	0.8	20	0.25	0.19	34
RS-7807	5357800	386400	0.1		0.07	0.6	0.17	9	1.1	9	0.13	0.06	29
RS-7808	5357810	386450	1		0.05	0.05	1.52	9	0.7	10	0.16	0.12	12
RS-7809	5357805	386500	2		0.06	0.6	3.87	9	0.7	10	0.17	0.19	14
RS-7601	5357600	386225	3		1.11	7.4	2.51	22	2.3	215	0.63	0.51	176
RS-7602	5357605	386275	0.1		0.43	1	2.51	10	0.9	33	0.25	0.17	41
RS-7603	5357600	386325	0.1		0.13	0.5	1.99	7	0.4	14	0.16	0.06	18
RS-7604	5357610	386375	2		0.14	0.7	0.61	7	0.8	12	0.23	0.05	43

RS-7605	5357600	386425	0.1		0.11	0.9	2.48	12	0.8	22	0.18	0.03	26
RS-7606	5357610	386475	0.1		0.09	0.7	1.89	14	0.9	40	0.32	0.07	16
RS-7607	5357605	386525	0.1		0.08	1.1	1.85	12	1	22	0.2	0.03	30
RS-7608	5357600	386575	0.1		0.08	0.8	0.47	14	1.8	18	0.21	0.09	18
RS-7609	5357600	386175	0.1		0.11	0.05	2.28	59	0.5	203	0.6	0.03	27
RS-7401	5357415	386251	0.1		0.5	4.1	2.57	11	1.6	113	0.47	0.53	76
RS-7402	5357400	386300	5		0.49	5.9	4.4	20	1.8	112	0.79	0.41	123
RS-7403	5357405	386350	6		0.51	4.9	1.16	28	1.6	320	0.74	0.49	109
RS-7404	5357400	386410	4		0.34	7.9	3.5	20	1.4	144	1.08	0.37	55
RS-7405	5357380	386460	0.1		0.11	0.9	2.65	11	1.1	18	0.36	0.15	24
RS-7406	5357400	386500	2		0.09	1.4	7.91	9	0.6	55	1.18	0.36	50
RS-7407	5357400	386555	5		0.05	1	4.7	11	1	21	0.28	0.08	10
RS-7408	5357400	386600	10		0.06	0.8	2.88	8	0.6	23	0.34	0.16	13
RS-7409			15	13	0.06	1.1	1.12	7	0.5	85	0.41	0.37	20
RS-7201	5357200	386325	2		0.22	157.3	2.15	43	5.1	361	1.39	2.75	521
RS-7202	5357215	386375	4		0.12	2	2.45	11	1.3	83	0.35	0.17	73
RS-7203	5357205	386425	2		0.11	3.4	0.44	8	0.9	141	0.22	0.19	126
RS-7204	5357200	386475	7		0.08	1.3	0.61	8	0.8	133	0.25	0.13	150
RS-7205	5357195	386530	5		0.08	1.7	2.27	12	1	60	0.21	0.17	19
RS-7206	5357200	386575	1		0.1	3	1.18	18	1.6	35	0.44	0.14	12
RS-7207	5357200	386625	2		0.07	1.1	1.92	14	1.1	27	0.29	0.15	19
RS-7208	5357200	386675	0.1		0.08	1.3	0.82	18	0.7	64	0.37	0.2	19
RS-7209	5357200	386725	13	18	0.07	1	3.22	8	0.8	57	0.37	0.34	30
RS-7210	5357195	386775	4		0.07	2.2	0.87	12	0.8	48	0.64	0.32	32
RS-7001	5357000	386400	0.1		0.06	0.8	1.09	15	1.1	39	0.63	0.08	24
RS-7002	5357005	386450	0.1		0.05	0.7	0.47	10	1	25	0.32	0.1	36
RS-7003	5357000	386500	98	44	0.11	1.8	1.57	8	1.2	153	0.2	0.21	68
RS-7004	5357000	386551	4		0.32	3.3	4.49	11	1.3	304	0.52	0.39	174
RS-7005	5357015	386600	7		0.36	2.1	0.98	13	1.4	681	0.35	0.33	140
RS-7006	5357020	386650	2		0.26	4.7	1.74	11	1.2	109	0.27	0.22	17
RS-7007	5357030	386700	8		0.15	11.6	0.76	10	0.9	38	0.37	0.25	26
RS-7008	5357030	386750	0.1		0.1	1.4	1.29	9	0.6	56	0.38	0.23	34

RS-7009	5357040	386800	0.1		0.08	0.6	1.11	7	0.7	15	0.41	0.24	15
RS-7010	5357000	386850	0.1		0.07	1.2	0.49	11	1	30	0.4	0.21	15
RS-6801	5356800	386425	0.1		0.09	4.9	0.71	21	1.1	64	0.76	0.04	21
RS-6802	5356800	386475	2		0.03	1	0.13	10	1.2	36	0.2	0.02	32
RS-6803	5356805	386525	0.1		0.07	1.9	0.25	10	0.9	19	0.5	0.15	28
RS-6804	5356800	386575	0.1		0.14	2.4	0.79	19	1.2	86	0.51	0.17	45
RS-6805	5356800	386625	2		0.13	8.1	0.68	11	1.2	114	0.42	0.35	54
RS-6806	5356800	386675	0.1		0.12	5.7	0.86	11	1.2	133	0.42	0.34	57
RS-6807	5356795	386725	1		0.19	13.8	0.77	31	1.6	273	0.7	0.46	304
RS-6808	5356805	386775	0.1		0.08	1.6	0.2	7	0.6	37	0.28	0.22	36
RS-6809	5356800	386825	0.1		0.06	1	0.2	8	0.7	22	0.4	0.27	30
RS-6810	5356800	386875	0.1		0.05	0.7	0.3	7	0.5	16	0.28	0.22	29
RS-6811	5356800	386925	0.1		0.05	1.1	0.17	9	0.6	54	0.46	0.28	32
RS-6812	5356795	386975	0.1		0.04	1.1	0.06	7	0.8	10	0.26	0.11	23
RS-6813	5356800	387025	0.1		0.09	2.2	1.32	27	0.9	155	1.04	0.07	31
RS-6814	5356800	387075	0.1		0.04	0.9	0.18	11	0.9	22	0.5	0.14	17
RS-6815	5356800	387125	0.1		0.04	0.7	0.96	7	0.9	9	0.29	0.12	12
RS-6601	5356605	386450	0.1		0.15	0.9	0.2	13	1.3	54	0.21	0.16	41
RS-6602	5356605	386500	0.1		0.15	2.4	0.31	12	1	54	0.55	0.23	30
RS-6603	5356600	386550	0.1		0.09	1.8	0.28	12	0.8	37	0.34	0.09	46
RS-6604	5356600	386600	0.1		0.11	5.7	0.65	17	0.9	50	0.53	0.29	25
RS-6605	5356610	386650	0.1		0.07	3.3	0.4	11	0.8	32	0.5	0.15	20
RS-6606	5356600	386700	0.1		0.05	1.7	0.25	8	0.8	24	0.43	0.14	22
RS-6607	5356600	386750	0.1		0.07	1.6	0.23	9	0.6	18	0.31	0.11	21
RS-6608	5356615	386800	0.1		0.08	1.5	0.23	11	0.8	82	0.42	0.15	88
RS-6609	5356610	386850	1		0.05	1.4	0.16	8	0.7	18	0.33	0.13	22
RS-6610	5356625	386900	2		0.08	1.3	0.13	9	0.8	16	0.27	0.13	23
RS-6611	5356640	386950	0.1		0.08	1.9	0.16	10	0.7	15	0.32	0.1	22
RS-6612	5356610	387000	1		0.03	0.05	0.02	4	0.01	3	0.1	0.04	7
RS-6613	5356605	387050	0.1		0.05	1.7	0.19	9	0.8	22	0.38	0.14	25
RS-6614	5356610	387100	0.1		0.05	2.1	0.16	9	0.9	19	0.37	0.16	22
RS-6615	5356610	387150	0.1		0.04	1.2	0.2	10	0.7	14	0.35	0.13	26

RS-6616	5356605	387200	0.1		0.06	2.4	0.29	14	1.2	18	0.44	0.12	14
RS-6617	5356600	387250	0.1		0.05	1.8	0.32	15	1	25	0.43	0.1	17
RS-6401	5356395	386475	1		0.17	3	0.22	8	1.1	24	0.36	0.28	19
RS-6402	5356395	386525	0.1		0.14	1.3	0.25	13	1.1	66	0.42	0.17	146
RS-6403	5356390	386575	2		0.1	0.05	0.27	8	0.7	49	0.24	0.11	110
RS-6404	5356400	386625	4		0.06	1.8	0.14	9	1	16	0.33	0.12	15
RS-6405	5356400	386675	0.1		0.05	1.8	0.24	8	0.7	26	0.47	0.15	17
RS-6406	5356405	386725	0.1		0.03	1.2	0.11	7	0.5	18	0.33	0.14	14
RS-6407	5356400	386775	0.1		0.06	1.7	0.23	59	1	27	0.39	0.14	30
RS-6408	5356395	386825	0.1		0.06	2.6	0.45	15	0.7	33	0.59	0.18	27
RS-6409	5356400	386875	0.1		0.06	1.9	0.27	10	1	20	0.35	0.11	17
RS-6410	5356405	386925	0.1		0.04	2.2	0.18	9	0.9	17	0.36	0.09	17
RS-6411	5356410	386975	3		0.07	1.6	0.38	13	1.2	34	0.45	0.08	17
RS-6412	5356430	387025	0.1		0.05	1.5	0.23	7	0.9	21	0.37	0.11	18
RS-6413	5356420	387075	5		0.04	1.5	0.22	8	0.9	20	0.26	0.08	20
RS-6414	5356430	387125	0.1		0.04	2.1	0.18	9	1.2	18	0.59	0.11	22
RS-6415	5356430	387175	0.1		0.04	3.2	0.28	10	1.1	22	0.61	0.17	26
RS-6416	5356430	387225	0.1		0.04	0.8	0.07	10	0.7	13	0.14	0.09	18
RS-6417	5356430	387275	7		0.05	1.6	0.16	8	1	14	0.32	0.11	15
RS-6418	5356425	387325	0.1		0.05	4.5	0.17	8	0.8	18	0.22	0.12	18
RS-6419	5356425	387375	0.1		0.04	2.1	0.21	11	1.1	21	0.33	0.12	19
RS-6201	5356205	386605	0.1		0.07	0.6	0.12	10	1.1	4	0.19	0.05	3
RS-6202	5356200	386650	0.1		0.06	1.7	0.22	13	1.1	18	0.32	0.13	14
RS-6203	5356190	386700	0.1		0.04	1.4	0.28	9	0.7	25	0.35	0.16	35
RS-6204	5356180	386750	0.1		0.05	1	0.11	8	1	13	0.3	0.14	12
RS-6205	5356200	386800	0.1		0.05	3.4	0.48	8	0.7	25	0.46	0.18	27
RS-6206	5356200	386850	0.1		0.06	5.4	0.49	10	0.8	31	0.47	0.12	19
RS-6207	5356200	386900	0.1		0.06	2.1	0.39	12	0.7	41	0.36	0.15	27
RS-6208	5356195	386950	1		0.05	2.6	0.31	9	1	22	0.36	0.16	21
RS-6209	5356200	387000	0.1		0.07	2.9	0.29	8	0.5	18	0.4	0.2	17
RS-6210	5356195	387050	0.1		0.09	1.2	0.15	8	0.9	24	0.3	0.15	40
RS-6211	5356190	387100	0.1		0.07	0.9	0.1	8	0.9	15	0.22	0.1	23

RS-6212	5356190	387150	0.1		0.06	1.8	0.13	7	0.8	15	0.27	0.11	25
RS-6213	5356190	387200	0.1		0.05	2.1	0.19	8	1	19	0.31	0.12	16
RS-6214	5356190	387250	0.1		0.05	1.4	0.35	9	1	41	0.39	0.18	36
RS-6215	5356190	387300	4		0.05	1.9	0.38	9	1.1	34	0.27	0.12	17
RS-6216	5356195	387350	0.1		0.07	4.2	1.05	16	1.3	57	0.69	0.15	26
RS-6217	5356200	387400	1		0.05	1.5	0.4	13	1	52	0.4	0.07	40
RS-6218	5356200	387450	5		0.05	1.6	0.27	9	1	33	0.38	0.1	35
RS-6001	5356000	386825	1		0.06	2	0.15	7	0.7	24	0.29	0.19	23
RS-6002	5355990	386875	0.1		0.06	1.7	0.5	9	0.9	20	0.31	0.18	22
RS-6003	5355990	386925	0.1		0.06	1.6	0.68	21	0.4	68	0.45	0.04	24
RS-6004	5355990	386975	1		0.05	1.5	0.27	10	0.8	18	0.26	0.1	30
RS-6005	5355995	387025	1		0.05	1.7	0.3	10	0.8	18	0.35	0.17	30
RS-6006	5355995	387075	0.1		0.25	6.3	0.36	12	1.3	29	1.51	0.17	71
RS-6007	5355995	387125	0.1		0.1	3.4	0.42	9	1.1	22	0.41	0.11	14
RS-6008	5355995	387175	0.1		0.06	1.6	0.24	10	1.2	14	0.41	0.12	15
RS-6009	5356005	387225	5		0.05	1	0.14	9	0.8	10	0.25	0.08	13
RS-6010	5356015	387275	1		0.04	1.7	0.22	9	1	13	0.53	0.12	18
RS-6011	5356005	387325	4		0.09	0.9	0.16	9	0.6	9	0.25	0.13	22
RS-6012	5356005	387375	0.1		0.08	1.6	0.31	7	0.7	28	0.37	0.12	27
RS-6013	5356010	387425	3		0.07	3.6	0.34	12	0.9	132	0.52	0.16	59
RS-6014	5356010	387475	0.1		0.06	1	0.1	10	1.4	19	0.24	0.12	19
RS-6015	5356010	387525	0.1		0.08	1.3	0.23	9	0.9	43	0.28	0.11	36
RS-6016	5356000	387570	8		0.16	1.1	1	9	0.9	175	0.34	0.28	52
RS-5801	5355805	386700	1		0.03	0.9	0.71	15	0.7	12	0.27	0.22	11
RS-5802	5355800	386750	0.1		0.07	2.6	0.89	22	0.8	28	0.4	0.09	16
RS-5803	5355800	386800	0.1		0.03	1.7	0.12	9	0.9	11	0.24	0.07	11
RS-5804	5355800	386850	0.1		0.04	1.5	0.22	12	1.6	20	0.4	0.28	26
RS-5805	5355810	386900	0.1		0.08	2.7	0.55	15	1	43	0.78	0.14	24
RS-5806	5355805	386950	0.1		0.05	5.8	0.48	16	1.5	16	0.35	0.17	32
RS-5807	5355800	387000	0.1		0.05	1.7	0.5	13	1.1	16	0.39	0.12	23
RS-5808	5355795	387050	0.1		0.05	2.8	0.51	12	0.7	28	0.51	0.09	15
RS-5809	5355790	387100	3		0.16	1.4	0.56	14	1.5	23	0.4	0.19	24

RS-5810	5355795	387150	1		0.1	1.5	0.27	11	1.1	19	0.35	0.1	23
RS-5811	5355790	387200	1		0.11	2.6	1.27	33	0.7	137	0.9	0.08	30
RS-5812	5355800	387250	4		0.08	3.5	0.69	13	1	31	0.51	0.14	16
RS-5813	5355800	387300	0.1		0.05	1.1	0.19	8	0.6	16	0.19	0.1	18
RS-5814	5355800	387350	0.1		0.05	1	0.29	14	0.9	27	0.21	0.11	17
RS-5815	5355805	387400	0.1		0.07	1.4	0.24	8	1.2	19	0.22	0.15	31
RS-5816	5355800	387450	5		0.14	0.6	0.43	7	0.6	69	0.19	0.23	62
RS-5817	5355800	387500	0.1		0.14	4.2	0.46	9	0.9	142	0.45	0.25	63
RS-5818	5355800	387550	5		0.16	0.6	1.17	11	0.8	97	0.26	0.18	52
RS-5819	5355800	387600	1		0.18	1.3	0.75	11	0.8	179	0.29	0.27	52
RS-5820	5355800	387650	1		0.15	3.5	0.18	7	0.5	112	0.28	0.35	41
RS-5821	5355805	387700	8		0.15	8.9	0.38	12	1.1	87	0.14	0.16	31
RS-5601	5355600	386625	6		0.05	2.5	0.31	12	1	22	0.25	0.12	9
RS-5602	5355580	386675	0.1		0.12	3.8	2.08	37	1.3	192	0.75	0.09	36
RS-5603	5355590	386725	1		0.04	2	0.46	10	1.1	28	0.43	0.11	11
RS-5604	5355600	386775	0.1		0.05	1.4	0.19	10	0.9	28	0.18	0.1	10
RS-5605	5355600	386825	0.1		0.04	1.1	0.07	9	1	9	0.26	0.09	10
RS-5606	5355600	386875	2		0.04	1.4	0.07	10	0.8	19	0.29	0.09	93
RS-5401	5355420	386550	7		0.08	3.9	40.62	10	2.4	109	0.2	0.05	119
RS-5402	5355410	386600	3		0.09	1.1	0.94	7	1	64	0.15	0.09	36
RS-5403	5355405	386650	4		0.07	1.7	0.33	7	0.6	48	0.14	0.1	35
RS-5404	5355400	386700	5		0.12	3.5	0.72	8	1.3	76	0.36	0.28	54
RS-5405	5355395	386750	0.1		0.09	1.4	0.35	14	0.9	49	0.42	0.17	41
RS-5406	5355410	386800	5		0.08	3.1	0.35	9	0.7	28	0.27	0.11	26

APPENDIX 3

(Six Monthly Report)

Geoinformatics Report

Probabilistic Targeting Using MOCA (Monte Carlo Targeting Software

Probabilistic targeting is a model-driven method of targeting for mineral deposits using Monte Carlo (MOCA) probabilistic algorithms. It uses a petroleum systems approach that divides the mineralizing system into components that could include source, host, pathway, focus and trap. The major advantages of probabilistic targeting over other methods are:

- uncertainty and risk are incorporated into the targeting procedure
- a wide range of scores are generated for a small number of input layers making only a few key layers necessary
- reduction to a few key input layers demands rigorous geological assessment of the deposit / exploration model and critical evaluation of the input datasets, which improves the integrity and fidelity of targeting
- it employs a multiplicative probabilistic scoring method in contrast to additive methods used by most other targeting methods, thereby reducing the number of false positives by eliminating areas that lack any of the key features
- it provides an effective method of ranking targets and, if employed consistently, should allow for comparison of targets across projects

The key parameters for 3D MOCA targeting are the interpreted **fundamental controls on the targeted mineralization systems and three-dimensional modelling of structural and lithological features** to enable spatial location of the generated targets.

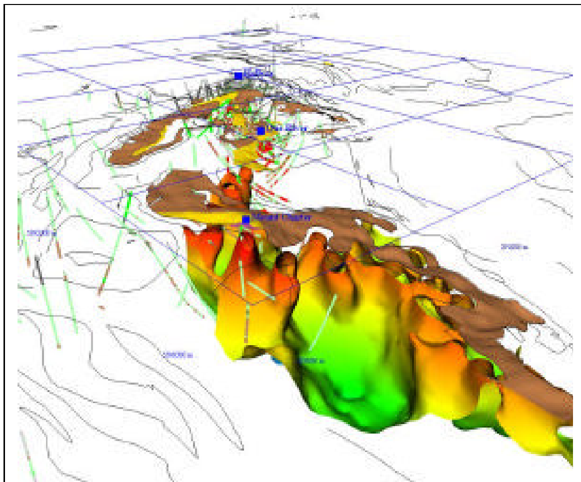
The controls on mineralization are derived from study of published literature, field observations, and observations made by other exploration companies released into the public domain.

Three-dimensional modelling of geology is constrained using geophysical data at both the local and regional scale. Magnetic and gravity inversions are coupled with available geological mapping and drill-hole data to create detailed local scale models whereas regional scale models incorporate analysis of the broader geophysical datasets.

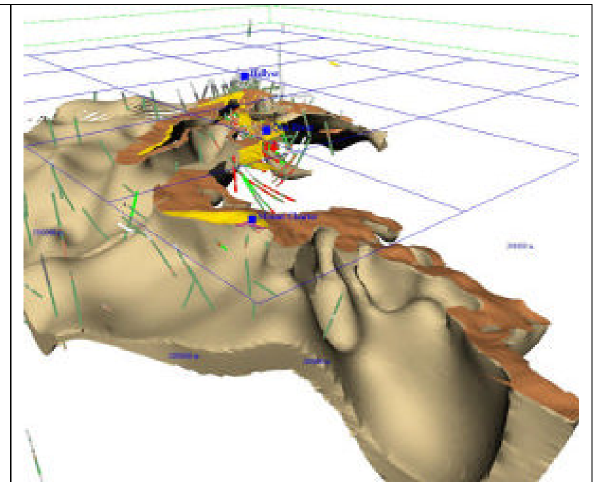
In order to construct the 3D probability grid, a number of probability and uncertainty parameters must be applied to the modelled features.

Each geological feature modelled has an associated **probability and uncertainty that the feature exists (Pex and Uex)**. Pex and Uex account for uncertainties in data quality and interpretation. The probability is related to how many other possible interpretations there are for the data. For example, if you have a small round anomaly in a magnetics survey you could have a small intrusive body, a zone of magnetite alteration, or even a building. If these three possibilities are equally likely, the Pex of an intrusion is 0.33. If there were mapped intrusions in this area, the Pex would be increased to reflect the higher likelihood of the magnetic anomaly being an intrusion. The uncertainty accounts for the quality of data being used for the interpretation. For example, an intrusion picked from a magnetic survey with 400m line spacing would get a higher uncertainty than one picked from a survey with 50m line spacing.

Each feature also has an associated **probability and uncertainty that the feature has the desired effect (Peff and Ueff).**



Magnetic inversion, interpreted geology at surface from mapping, and geological log-data in drill-holes



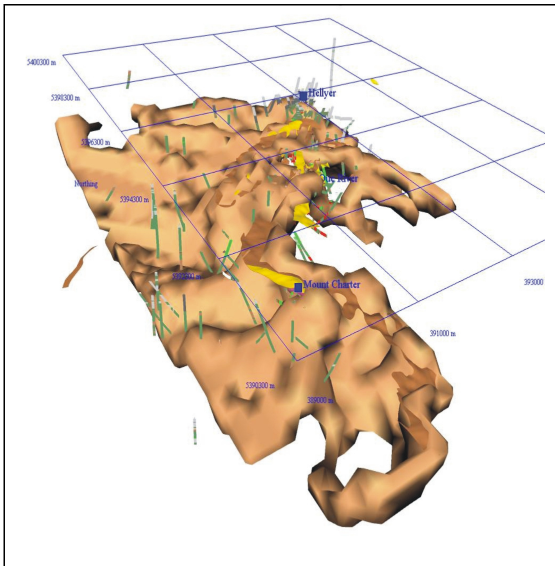
Resulting 3D geological model constructed by combining all available data types

For example, when trying to estimate the probability that a certain fault is a pathway for mineralising fluids, Pex is the probability that a fault is present and Peff is the probability that the fault carried mineralising fluids. In this case the Peff could be higher for faults in a dilational syndepositional orientation (e.g NNE) at the time of mineralisation or it could be higher for faults with evidence of geochemical anomalies. The Ueff is an estimate of how well we can constrain the Peff. The Peff and Ueff are often subjective and it is unlikely that they will be correct values. However, relative estimates of these values should be possible. This implies that the actual values for the final probabilities for each layer and the probability of success will be approximate but that relative values should be valid.

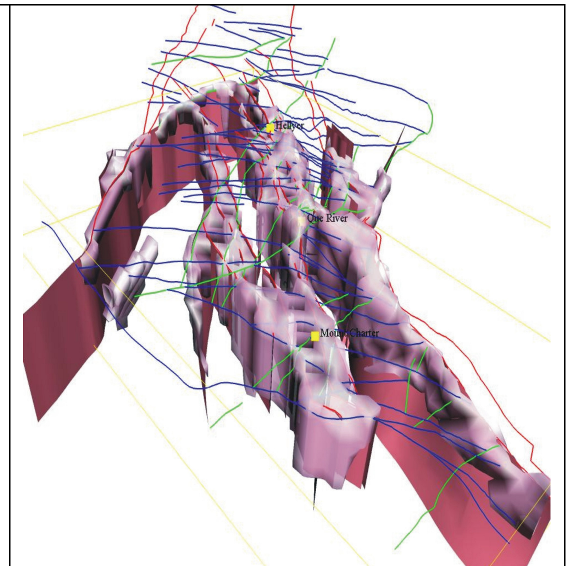
An area of influence (AOI) is a buffer that is applied to each object when it is placed on the final output grids. This is applied because a given feature could influence a larger area than its mapped extent. For example, a fault on a map may actually comprise a structural zone with a wider influence on surrounding host rocks than suggested by a simple line on a map. The slope is the amount of probability to drop per kilometre after the AOI. This reflects the decreasing effect of an object as you move away from it and also tries to account for spatial uncertainty. The slope is reported in units of per km because the probability does not have any units. So a slope of 0.5/km indicates that the probability will be zero 2 km away from the AOI. The slope for an object is not constant because the spatial uncertainty is dependent on how well constrained an interpretation is. So if a unit that is pierced by drill holes will have a steeper slope near the drill holes and a broader slope away from them. Results from the MOCA targeting are presented on 3D probability grids. The targeting uses output probability grids with a 100m and 200m grid cell size.

To generate three-dimensional targets, the geological framework and probability grid is interrogated based on the four components of **host, pathway, focus, and trap**.

From earlier compilation of published interpretations and interpretations of the open-file data, the key **host** rocks to particular mineralization systems are identified. The probability grid can be filtered to show areas of higher probability that the host stratigraphy is present.



Pex of 50% for modelled host stratigraphy



Pex of 50% for fluid pathways defined by structures

Similarly, key structures interpreted as fluid conduits for mineralizing fluids are assigned buffer zones or areas of influence. Intuitively, areas of intersection of these **pathway** zones with host stratigraphy are the broader target areas.

Other features interpreted as integral in the localization of mineralization such as cross-cutting faults or folds are also assigned areas of influence and each structure continues to retain its original Pex/Peff. This represents the **focus** input layer.

The **trap** input layer incorporates evidence that the target metal/sulphides were precipitated within a preferred host horizon. The primary consideration for the trap site is therefore the recognition of geological, geochemical, and/or geophysical evidence for metal precipitation.

Three datasets respectively were chosen to test for trap sites;

- Drilling data with recorded evidence of sulphide precipitation, either directly observable or reflected in assay analyses,
- Surface geochemical data including C-horizon soil sampling, MMI analyses, rock-chips or stream sediment sampling,
- Ground and airborne electromagnetic (EM) data to test for coherent massive sulphide material providing sufficient electrical continuity and conductivity to directly indicate a VHMS trap environment.

Both the drilling and geochemical data can be considered discontinuous datasets and not amenable to the production of ubiquitous gridded coverage across the modelled region. Consequently, these data were used adjunctively to test for multivariate metal anomalism at each Host-Pathway-Focus (HPF) site generated by the 3D MOCA targeting algorithm.

Probabilities of existence and effect are multiplied as such to give a probability of success for each given target area. These are directly comparable with other targets and the method thereby acts as a transparent ranking tool in terms of prospectivity.

Modified from a description of the Geoinformatics Inc. MOCA process supplied by Dan Core and Graeme Cameron from that company.